# Structure Investigation Report Proposed Four Mile Creek Culvert Modification South Trade Street Mecklenburg County, North Carolina TIP Project No. U-5025 S&ME Project No. 1351-08-001B

#### **Prepared For:**

The Town of Matthews
Public Works Department
1600 Tank Town Road
Matthews, North Carolina 28105

#### **Prepared By:**



S&ME, Inc. 9751 Southern Pine Blvd. Charlotte, North Carolina 28273 NC PE Firm License No. F-0176



April 19, 2010

The Town of Matthews Public Works Department 1600 Tank Town Road Matthews, North Carolina 28105

Attention: Mr. Ralph Messera

Reference: Structure Investigation Report

Proposed Four Mile Creek Culvert Modification

South Trade Street

Mecklenburg County, North Carolina

TIP No.: U-5025

S&ME Project No. 1351-08-001B NC PE Firm License No. F-0176

Dear Mr. Messera:

S&ME, Inc. has completed the subsurface exploration of the referenced project site. The purpose of this study was to determine the subsurface conditions along the proposed new culvert alignment, so that those conditions can be evaluated regarding the appropriate foundation and construction considerations for the culvert extension over Four Mile Creek.

This report presents S&ME's findings of our investigation and foundation recommendations. Included in the Appendix are a Site Vicinity Map, Field Exploration Plan, Generalized Subsurface Profile along the west end of the proposed culvert structure, Generalized Subsurface Profile along the east end of the proposed culvert structure, Generalized Subsurface Profile along the proposed culvert extension, Generalized Subsurface Profile along the proposed culvert extension, Generalized Subsurface Profile along the proposed pedestrian tunnel, Boring Logs, Rock Core Photographs, Site Photographs and a Field Scour Report.

S&ME appreciates the opportunity to assist you during this phase of the project. If you should have any questions concerning this report or if we may be of further assistance, please contact us.

Very truly yours, S&ME, Inc.

Luis A. Campos, E.I. Staff Professional

Duane D. Bents, P.E.

Geotechnical Services Manager

N.C. Registration No. 31525

Senior Review by: Kristen H. Hill, P.E., P.G. Senior Geotechnical Engineer

LAC/DDB/KHH/cs

S/1351/Project/2008/08-001B

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#### **SECTION 1000**

#### **GEOLOGIC INVENTORY REPORT**

#### 1010 Project Description

We understand that plans are to widen S. Trade Street (SR 3448) from a two-lane roadway to a four-lane roadway with a bicycle lane between its intersection with John Street (SR 1009) and Weddington Road (SR 3468) in Mecklenburg County, North Carolina. To facilitate the widening, the bottomless culvert at the crossing of Four Mile Creek must be modified and/or replaced.

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Based on the most recent information provided to us by Kimley-Horn and Associates, Inc., we understand that the proposed structure will be lengthened to a total length of approximately 180 feet in the generally east and west directions. In addition, a pedestrian tunnel is proposed approximately 30 feet south of the existing culvert. The culvert extension will be cast-in-place concrete construction with an opening slightly larger than the existing structure. The structure will include concrete wing walls that will tie into the pedestrian tunnel wing walls.

#### 1020 Site Description & Geology

The project site is located in Mecklenburg County, North Carolina, at the crossing of Four Mile Creek just south of Chaphyn Lane and north of Brenham Lane. At this crossing, Four Mile Creek runs approximately east-west and S. Trade Street runs approximately north-south. The subject bottomless arched culvert is about 90 feet in length with a width of about 24 feet and a height of about 15 feet. The roadway elevation is approximately 15 feet higher than the top of the culvert, resulting in an approach embankment height of about 30 feet. Based on topographic information in the culvert area provided to us, the embankment slope is approximately 1.2H:1V on both sides of Trade Street. Visual observations suggest a slightly steeper slope directly above the culvert. The embankment slopes are covered with underbrush and small trees.

The culvert site is located within the Charlotte Belt of the Piedmont Physiographic and Geologic Province of North Carolina. The Piedmont Province generally consists of well-rounded hills and ridges, which are dissected by a well-developed system of draws and streams. The Piedmont Province is predominantly underlain by metamorphic rock (formed by heat, pressure and/or chemical action) and igneous rock (formed directly from molten material), which were initially formed during the Precambrian and Paleozoic eras. The volcanic and sedimentary rocks deposited in the Piedmont Province during the Precambrian eras were the host for the metamorphism and were changed to gneiss and schist. The more recent Paleozoic era had periods of igneous emplacement, with at least several episodes of regional metamorphism resulting in the majority of the rock types seen today.

The topography and relief of the Piedmont Province have developed from differential weathering of the igneous and metamorphic rock. Because of the continued chemical and physical weathering, the rocks in the Piedmont Province are now generally covered with a mantle of soil that has weathered in place from the parent bedrock. These soils have variable thicknesses and are referred to as residuum or residual soils. The residuum is typically finer grained and has a higher clay content near the surface because of the advanced weathering. Similarly, the soils typically become coarser grained with increasing depth because of decreased weathering. As the degree of weathering decreases, the residual soils generally retain the overall appearance, texture, gradation and foliations of the parent rock. Alluvial soils, consisting of interbedded sands, silts, and clays, are common in the floodplain along rivers and creeks in the Piedmont.

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#### 1030 Field Testing

A combination of soil test borings, hand augers with Dynamic Cone Penetrometer (DCP) testing, and bridge rod soundings were used to determine the subsurface conditions in the vicinity of the existing culvert. The field exploration methods were performed in accordance with the "NCDOT Geotechnical Unit Guidelines and Procedures Manual", revised March 1994.

The soil test boring, hand auger boring and bridge rod sounding locations were determined in the field by S&ME staff professionals. The test locations are presented relative to corresponding stations and offsets from the -L- survey line. Ground surface elevations indicated on the test logs were determined through a differential level survey referenced to Benchmark (BM-242) with an elevation of 648.77 feet-MSL. The Benchmark was provided to us by Sanborn and is identified as a metal nail set into the sidewalk on the west side of S. Trade Street, south of the subject creek.

#### 1031 Soil Test Borings

Soil test borings were conducted from January 20 through 25, 2008 and from January 8 through 13, 2009. Fourteen borings (designated B-1 through B-8 and BB-1 through BB-6) were drilled by S&ME personnel along the existing roadway in the vicinity of the culvert, near the proposed culvert corners and along the proposed pedestrian walkway as shown on the Field Exploration Plan (Sheet No. 4). The borings were drilled with a CME-45B drill rig mounted on a truck carrier as well as a CME-550x and Mobile BK-51 drill rigs mounted on all-terrain vehicles. The borings were advanced to depths ranging from 2.4 to 37.5 feet (elevations 636.6 to 596.9 feet).

All of the borings were penetrated using hollow stem auger procedures (either 2-1/4 inch or 3-1/4 inch) onto crystalline rock or, in the case of Boring B-3, onto the concrete surface of the culvert arch. Standard penetration tests were performed in accordance with AASHTO T206-87 in all of the borings. Rock coring was performed in selected borings.

#### 1032 Hand Auger Borings with DCP Testing

On January 25, 2008, S&ME personnel performed six (6) hand auger borings (designated HA-1 through HA-6) with Dynamic Cone Penetrometer (DCP) testing at approximate locations shown on the Field Exploration Plan in the Appendix; no ground surface

penetration was possible at the hand auger boring location HA-3 due to the presence of rip rap. The hand auger borings were advanced to depths ranging between 1.2 and 5 feet below the existing ground surface. The DCP tests were performed at 1 foot intervals, beginning at the ground surface.

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#### 1033 Bridge Rod Soundings

On February 5, 2008, S&ME personnel performed twelve (12) bridge rod soundings (designated BR-1 through BR-15) at approximate locations shown on the Field Exploration Plan. The bridge rod soundings were advanced to depths ranging between 0.7 and 5.7 feet below the existing ground surface except for BR-9 and BR-13 where no sounding rod penetration was possible.

#### 1040 Laboratory Testing

One undisturbed soil sample was collected from Boring B-4 and a consolidated undrained (CU) triaxial compression test was planned, however, the sample did not remain intact during sample extrusion. Additional laboratory testing of representative soils samples was completed to determine the soil index properties and to verify field classifications. This samples were analyzed for grain size distribution (including hydrometer) (T88-90), determination of liquid limit (T89-90), plastic limit and plasticity index (T90-87) with NCDOT modifications. Laboratory test results are presented in the appendix.

#### 1050 Subsurface Conditions

The test borings indicate relatively uniform subsurface conditions at the proposed culvert extension location with some non-conformity with respect to stratigraphic correlations along the proposed alignment as indicated on the attached Generalized Subsurface Profiles (see Sheet Nos. 5 through 8). The descriptions of the subsurface conditions in the following paragraphs are based on conditions encountered in the soil test borings. The Generalized Subsurface Profiles were developed by S&ME personnel utilizing surveying techniques referencing the benchmark provided and existing site features. In addition, detailed descriptions of the conditions encountered at the individual test boring location are presented on the attached Boring Logs.

#### 1051 Fill Materials

Roadway embankment fill and artificial fill materials were encountered in each of the borings, with the exception of Borings B-5 and B-6, to depths of about 2.4 to 32 feet (elevations 636.6 to 609.3 feet) beneath the collar elevations. The fill materials encountered consist of medium dense brown silty sand (A-2-4), soft to very stiff red brown tan fine sandy silt (A-4), stiff brown fine sandy silt (A-5), medium stiff to very stiff red brown clayey silt (A-7-5) and stiff tan silty clay (A-7-6). Standard penetration test (SPT) N-values in the fill soils ranged from 4 blows per foot (bpf) to 62 blows per 0.7 feet of penetration.

#### 1052 Alluvial Deposits

Alluvial deposits were encountered underlying roadway embankment and artificial fill soils in Borings B-2, B-4, BB-2, BB-3, BB-5 and BB-6 to depths ranging from about 6 to 37.5 feet (elevations 617.1 to 609.9 feet) beneath the collar elevations. The alluvial deposits encountered in the borings consist of medium stiff gray brown fine sandy silt (A-4), stiff brown clayey silt (A-6), very soft to soft gray brown sandy silty clay (A-7-6), very loose to medium dense gray brown silty fine to coarse sand (A-2-4) and very loose brown gray clayey fine sand (A-2-7). The SPT N-values in the alluvium ranged from Weight-of-Hammer (WOH) to 17 bpf.

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#### 1053 Residuum

Residual materials exist beneath the topsoil in Boring B-5 as well as beneath alluvial deposits in Borings BB-2 and BB-5. The residuum generally consisted of very stiff red tan brown clayey silt (A-7-5) and dense to very dense white tan brown silty fine to coarse sand (A-2-4). The SPT N-values in the residuum ranged from 29 to 91 bpf.

Weathered rock was encountered beneath the alluvial deposits in Boring BB-5, beneath residual soils in Borings B-5 and BB-6, and beneath topsoil in Boring B-6. The surface of the weathered rock was encountered at depths of about 0.5 to 13 feet (elevations 636.9 to 609.9) feet beneath the collar elevations. The weathered rock materials were penetrated by hollow stem augers to depths of 0.3 to 14.3 feet (elevations 631.3 to 608.6 feet) beneath the collar elevations. The SPT N-values in the weathered rock materials ranged from 100 blows per 0.6 feet of penetration to 60 blows per 0.1 feet of penetration.

The weathered rock transitions to crystalline rock consisting of gray brown granodiorite. Crystalline rock exists directly beneath fill soils in Borings B-7, B-8, BB-1 and BB-4, directly beneath alluvial soils in Borings B-2, B-4 and BB-3, and directly beneath residual soils in Borings B-5, B-6, BB-2, BB-5 and BB-6. The surface of crystalline rock was encountered at depths ranging from 2.4 to 37.6 feet (elevations 631.3 to 608.6 feet) beneath the collar elevations. The crystalline rock was evaluated utilizing rock coring techniques by advancing an NQ-2 core barrel. The recovered core samples were generally classified as medium hard to hard, moderately weathered to very slightly weathered, brown gray, with close to very close fracture spacing. Core activities recovered 76 to 100 percent of to crystalline rock cored. Rock Quality Designations (RQD) values ranged from 10 to 87 percent. Borings BB-5 and BB-6 were terminated in hard granodiorite at elevations of 596.9 and 599.9 feet, respectively. Borings B-2, B-4 through B-8, BB-1, BB-3 and BB-4 were terminated on crystalline rock at elevations ranging from 631.3 to 609.3 feet.

#### 1060 Groundwater

Groundwater was measured in Borings B-2, B-4, B-7, BB-5 and BB-6 at depths of 7 to 37 feet below the existing ground surface (approximate elevations of 611.8 to 616.2 feet-MSL) at the respective boring terminations. Water levels were measured after a stabilization period of at least 24 hours in Borings BB-3, BB-5 and BB-6 at depths of 3 to 8 feet below the existing ground surface (approximate elevations 614.9 to 617.5 feet-

MSL). The remainder of the borings performed for this study were either dry when water level measurements were attempted or backfilled due to safety concerns. All of the initial borings (Borings B-1 through B-8) were backfilled with soil cuttings on or before January 25, 2008. All of the secondary borings (Borings BB-1 through BB-6) were backfilled with soil cuttings on or before January 14, 2009. The creek level at the time of our exploration was at approximately elevation 614 feet-MSL.

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Please note that groundwater levels tend to fluctuate with seasonal and climatic variations, as well as with some types of construction operations.

#### 1070 Scour

A field scour report was conducted for the proposed culvert on S. Trade Street over the Four Mile Creek site as part of this phase of the project. The scour field observations were performed on March 27, 2008 and the scour report is included in the Appendix of this report.

#### **SECTION 2000**

#### **FOUNDATION RECOMMENDATIONS**

#### 2010 Foundation Support

We understand that the culvert extensions will be approximately 18 foot by 16 foot cast-in-place bottomless structures. Based upon our subsurface exploration, the average elevation of the top of crystalline rock is at about an elevation of 613 feet on the downstream end, and at about elevation 613.5 feet on the upstream end of the proposed culvert alignment. Foundations for the culvert should bear on crystalline or weathered rock where present. The culvert shall be designed for an allowable bearing pressure of 4 tons per square (tsf), which should be verified in the field.

Total and differential settlements along the proposed culvert alignment are anticipated to be less than ¼ inch if constructed on weathered rock or crystalline rock.

Along the proposed pedestrian tunnel alignment, the elevations of the top of crystalline rock ranged from an elevation of about 616.4 feet to lower than 613.1 feet. Based on the provided plans, head wall and wing wall foundations for the pedestrian tunnel will bear at elevations ranging between 627.62 and 621.12 feet-MSL. In order to limit differential settlements, we recommend that foundation soils be undercut to a depth of 2 feet or an elevation of 623.5 feet-MSL, whichever is deeper. Isolated, deeper undercutting may be required to remove excessively soft foundation soils. Undercut material shall be replaced with material that meets the requirements of Select material Class III in accordance with Section 1016 of the Standard Specifications. The material shall be compacted to a minimum of 95% of the maximum dry density as determined by AASHTO T-99. Once the site improvements have been completed, the foundation soils for the head walls and wing walls shall be suitable for walls designed using a bearing pressure of 2 tsf.

Total settlements for the head walls and wing walls are anticipated to be less than 1 inch if the undercut recommendations are implemented. Differential settlements between adjacent head walls and wing walls should be less than ½ inch.

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Depending upon the creek level, dewatering of up to 5 feet may be required for construction of the shallow foundation system. Foundation construction should be performed on one side of the creek at a given time. The existing creek should be temporarily dammed and water pumped away from the construction area. Cased sumps with submersible pumps may be required within the excavation. As the excavation to adequate and level bearing materials for the foundation proceeds, pumping from the cased sumps should be maintained to de-water the excavation.

The proposed roadway construction will require up to approximately 20 feet of fill placement in the subject culvert and pedestrian tunnel areas. Settlement resulting from the loading associated with fill placement is anticipated within newly placed embankment soils and underlying bearing soils where embankment construction will occur. It is anticipated that the majority of settlement of these materials will occur during placement of the new embankment fill. To reduce maintenance and repair of the approach fill, placement of roadway embankment shall be performed soon after construction has started to allow at least a 1-month waiting period for settlement of the embankment to occur prior to placement of the surface course. This will help to prevent delays in the completion of the project.

#### **SECTION 3000**

#### **QUALIFICATIONS OF REPORT**

This report has been prepared in accordance with generally accepted geotechnical engineering practice for specific application to this project. The conclusions contained in this report were based on the applicable standards of our profession at the time this report was prepared. No other warranty, expressed or implied, is made.

The conclusions submitted in this report are based, in part, upon the data obtained from the subsurface exploration. The nature and extent of subsurface variations between the borings may not become evident until construction. If variations appear evident, then the conclusions contained in this report may need to be re-evaluated. In the event that any changes in the nature, design, or location of the structure are planned, the conclusions contained in this report will not be considered valid unless the changes are reviewed by S&ME, and the conclusions of the report are modified or verified in writing.

#### FOUNDATION RECOMMENDATION NOTES AND COMMENTS

**TIP No.** <u>U-5025</u>

**Description**: S. Trade Street Culvert over Four Mile Creek

County: Mecklenburg

**Station**: 102 + 90 -L- Reinforced Concrete Bottomless Culvert @ 90° Skew

**Design:** LAC/DDB

**Date:** <u>4/19/2010</u>

LOCATION NO.	STATION	FOUNDATION TYPE	ALLOWABLE LOAD	MISCELLANEOUS DETAILS
1 West Side of Culvert	102 + 90 -L-	Concrete Wall Footing	4.0 tons/square ft.	Min. Culvert Bottom Elev.: 613
2 East Side of Culvert	102 + 90 -L-	Concrete Wall Footing	4.0 tons/square ft.	Min. Culvert Bottom Elev.: 613.5

#### **NOTES**:

- 1. The required bearing capacity of the culvert foundation along the length of the culvert is 4.0 tsf. Check field conditions for the required bearing capacity just prior to placing concrete.
- 2. Backfill with material that meets the requirements of Select Material Class VI in accordance with Section 1016 of the Standard Specifications.
- 3. The scour critical elevation for the culvert is the bottom of footing. The scour critical elevations are used to monitor possible scour problems during the life of the structure.
- 4. To provide protection from possible scour, do not construct culvert foundation along the length of the culvert at an elevation higher than shown on the plans.

#### FOUNDATION RECOMMENDATION NOTES AND COMMENTS

**TIP No.** <u>U-5025</u>

**Description**: S. Trade Street Culvert over Four Mile Creek

County: Mecklenburg

Station: 102 + 52 -L- Pedestrian Tunnel @ 90° Skew

**Design:** LAC/DDB

**Date:** <u>4/19/2010</u>

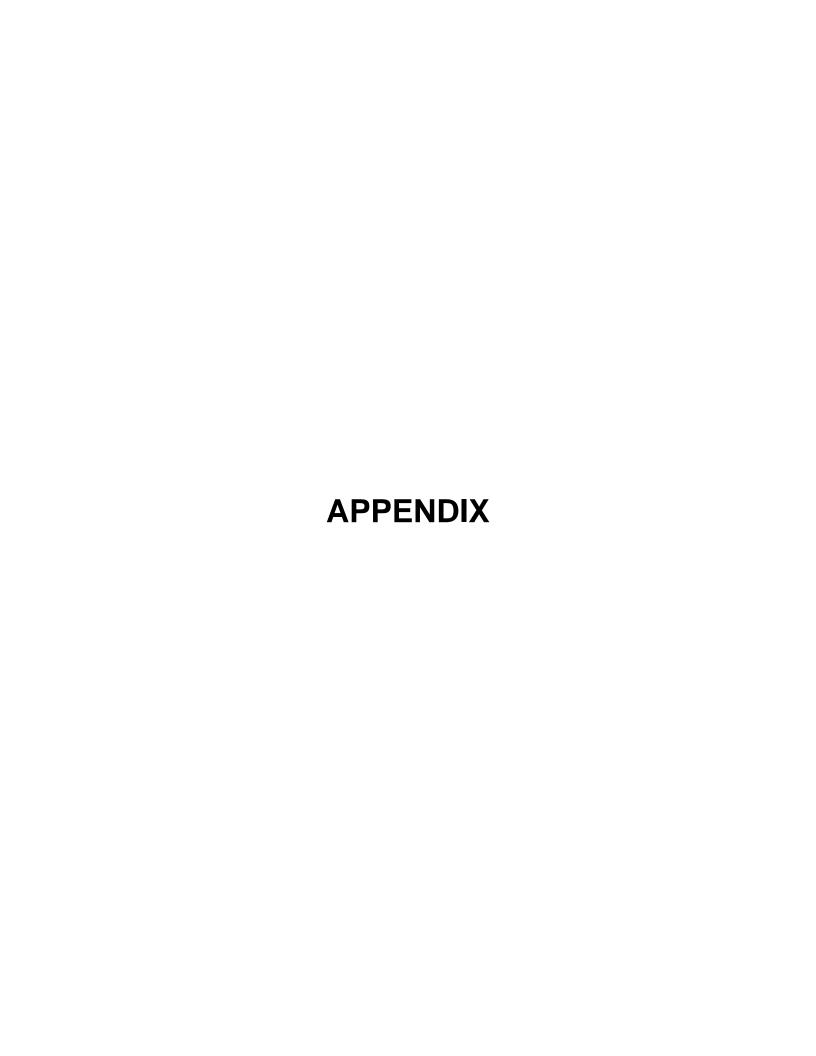
LOCATION NO.	STATION	FOUNDATION TYPE	ALLOWABLE LOAD
1 West Side of Tunnel	102 + 52 -L-	Concrete Head Wall and Wing Wall Footing	2.0 tons/square ft.
2 East Side of Tunnel	102 + 52 -L-	Concrete Head Wall and Wing Wall Footing	2.0 tons/square ft.

#### NOTES:

- 1. The required bearing capacity of the foundations bearing in soil is 2.0 tsf. Check field conditions for the required bearing capacity just prior to placing concrete.
- 2. Backfill with material that meets the requirements of Select Material Class III in accordance with Section 1016 of the Standard Specifications.
- 3. No work shall be done on the head walls and wing walls bearing on soil until the area of the head wall and wing wall foundations have been undercut to suitable bearing material and unsuitable/alluvial material replaced with suitable material properly compacted to the elevation of the bottom of the proposed head wall and wing wall foundations. The limits of this undercut excavation shall be to a depth of 2 feet or and elevation of 623.5 feet, whichever is deeper.
- 4. Scour protection consisting of rip rap in front of tunnel wing walls is required.

#### **General Comments**

- 1. Temporary shoring may be required for the culvert and wall construction.
- 2. Temporary cofferdams may be required for construction of culvert foundations.
- 3. No waiting period is required for the culvert or wall construction.
- 4. A 1-month waiting period after roadway embankment placement is required before the placement of the surface course.



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#### STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION

DIVISION OF HIGHWAYS

GEOTECHNICAL ENGINEERING UNIT

### STRUCTURE SUBSURFACE INVESTIGATION

WBS NoI.D. NO.U-5029	5
F.A. PROJECTCOUNTYMECKLENBURG	_
PROJECT DESCRIPTION S. TRADE STREET	
ROADWAY WIDENING - MATTHEWS, NC	_
SITE DESCRIPTION SITE 1: PROPOSED ARCHED	 )
BOTTOMLESS CULVERT EXTENSIONS OVER	
FOUR MILE CREEK AND PEDESTRIAN TUNNEL	

#### CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WAS MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORBING LOCS, ROCK CORES, AND SOLI TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL UNIT 0 (918) 250—4088. NEDTHER THE SUBSURFACE PLANS AND REPORTS, NOR THE FIELD BORING LOCS, ROCK CORES. OR SOLI TEST DATA IS PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORNESS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN STU (N-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DESCRIPE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOSTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS WOUNTING SOULDING CONDITIONS MOLUDING SOIL TIME TIME ACCORDING TO CLUMATIC CONDITIONS INCLUDING TEMPERATURES, PRECENTATION AND WIND, AS WELL AS OTHER NON-CLUMATIC FACTORS.

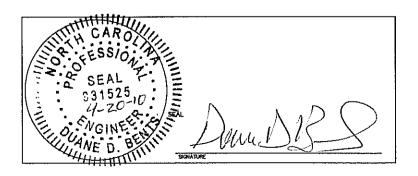
DEDCOMMEN D RENTS

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL BESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PUANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE OR OPINION OF THE DEPARTMENT AS TO THE THYE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DIEDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DIEDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DIEDER OR CONTRACTOR IS AND CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INFORMATION.

- NOTE THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS BEING ACCURATE NOR IT IS CONSIDERED TO BE PART OF THE PLANS, SPECIFICATIONS, OR CONTRACT FOR THE PROJECT.
- NOTE BY HAVING REQUESTED THIS INFORMATION THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS
  FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE
  CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

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DUANE D. BENTS		Z. SCARBORO
S&ME, INC.		M. LONGSHORE
3 /31 /2010		L. CAMPOS
	•	T. MILLER
	·	C. ODOM
	·	J. LITTLE
		C. DEESE
	DUANE D. BENTS S&ME, INC.	DUANE D. BENTS S&ME, INC.

SAME INC.



STATE	STATE PR	Э.	SHEET NO.	TOTAL	
NC			1B	51	
W	BS NO.	F.A. PROJ. NO.		DESCRIP	TION
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#### STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

## STRUCTURE SUBSURFACE INVESTIGATION

WBS No.\_\_\_\_\_\_\_I.D. NO.U-5025
F.A. PROJECT\_\_\_\_\_\_
COUNTY\_\_\_\_MECKLENBURG
PROJECT DESCRIPTION S. TRADE STREET
ROADWAY WIDENING - MATTHEWS, NC

SITE DESCRIPTION SITE 1: PROPOSED ARCHED
BOTTOMLESS CULVERT EXTENSIONS OVER
FOUR MILE CREEK AND PEDESTRIAN TUNNEL

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# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL UNIT SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

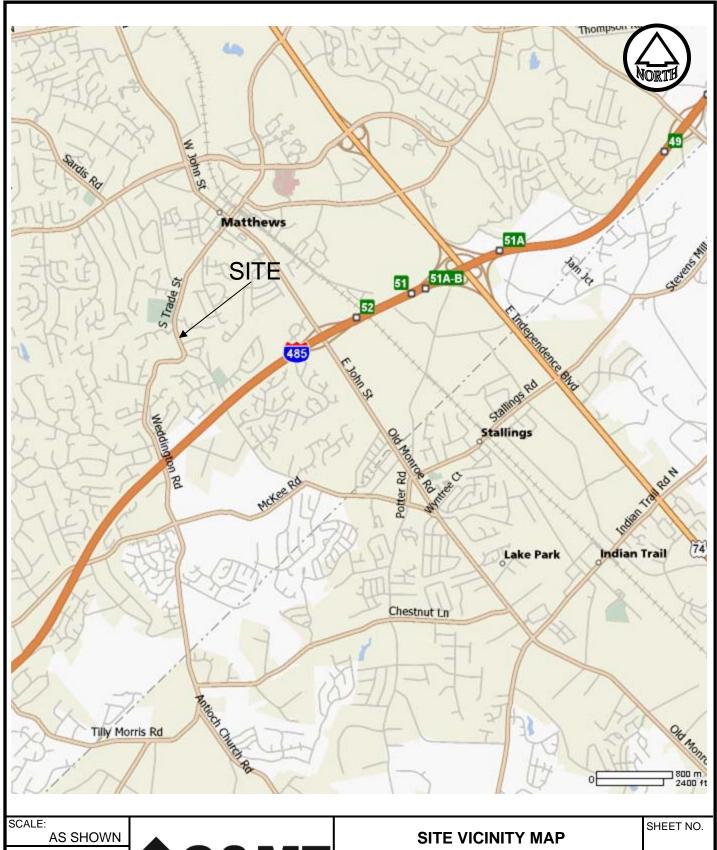
SOIL DESCRIPTION  SOIL IS CONSIDERED TO BE THE UNCONSOLIDATED, SEMI-CONSOLIDATED OR WEATHERED EARTH MATERIALS											WELL GRAF	DED- INF	DICATES A GO	OOD REPR	ESENTATI	GRADA ON OF PAI	RTICLE SIZES FI	ROM FINE	E TO COARSE			
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100 BLOWS	PER FOOT A	CCORDII	NG TO ST	ANDAR	D PENETR	ATION T	EST (A/	ASHTO	T206,	ASTM D-158 ALLY SHALL	36). SOIL		GAP-GRADED- INDICATES A MIXTURE OF UNIFORM PARTICLES OF TWO OR MORE SIZES.									
CONSISTENC	Y, COLOR, T	EXTURE,	, MOISTUR	E, AAS	SHTO CLAS	SSIFICAT	10N, AN	D OTH	er pei	RTINENT FACT			ANGULARITY OF GRAINS THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS ARE DESIGNATED BY THE TERMS: ANGULAR.									
AS MINERAL											-6				OR ROUNDNE ROUNDED, OR			S ARE DES	DIGNATED BY T	nt IEKM	o; MNGULAK,	
VERY STIFF, GRAY SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6 SOIL LEGEND AND AASHTO CLASSIFICATION											-					GICAL C	COMPOSITI	ON				
GENERAL			R MATER		ID AA	_	CLAY MA				NIC MATER	NAI S	MINERAL N	AMES SL	JCH AS QUAR	RTZ, FELD	SPAR, MIC	CA, TALC,			IN DESCRIPTIONS	
CLASS.			SSING #			+ -	% PASSI						WHENEVER	THEY A	RE CONSIDERI	ED OF SI						
GROUP CLASS.	A-1-a A-1-i	A-3	4 2 4 4	A-2	-2-6 A-2-	+	A-5	A-6	A-7-5	A-1, A-2 A-3	A-4, A-5 A-6, A-7	5		CLICATI	Y COMPRESSI	IDI E	COM	PRESS	IBILITY LIQUID LIMI	T LECC 1	DIAN 30	
SYMBOL	800000000	8	A-2-4 A	2-5 A	-2-6 A-2-		1646	$\overline{Z}$	A-7-6		,			MODERA	TELY COMPRE	ESSIBLE			LIQUID LIMI	T 31-50		
	888888888	8::::::												HIGHLY	COMPRESSIBL		DOENT	ACE O	F MATERI.		ER THAN 50	
	50 MX									GRANULAR	SILT- CLAY	MUCK,	0004	NIO MAT	FDIAL	GRANUL		LT-CLAY	T MAILIN			
	30 MX 50 M 15 MX 25 M					Jze 141	76 UNI	36 MM	36 MM	SOILS	SOILS	PEAT	TRACE OF	NIC MAT		SOILS 2 - 3		SOILS - 5%			ER MATERIAL	
LIQUID LIMIT	10 111/20 111	10 1111		$\neg$		1						1	LITTLE ORG	SANIC MA	ATTER	3 - 5	% 5	- 12%		TRACE LITTLE	1 - 10% 10 - 20%	
PLASTIC INDEX	6 MX	N.P.			MX41 MI MN 11 MI					SOILS '		l <u>.</u>	MODERATE		NIC	5 - 10% >10%		2 - 20% >20%		SOME HIGHLY	20 - 35% 35% AND ABOVE	
GROUP INDEX	0	0	6	$\neg$	4 MX	8 MX	12 MX	16 MX	No MX	MODER	ATE	HIGHLY							WATER		COM AND ADOVE	
USUAL TYPES		FINE	SILTY	OR C	LAYEY	SIL	ΤΥ	CLA	YEY	AMOUN ORGAN		SOILS	$\nabla$		WATER LE	EVEL IN I			ATELY AFTER	DRILLING	).	
OF MAJOR MATERIALS	GRAVEL AND SAND	SAND			D SAND	SO		SOIL		MATTER			<b>▼</b>					r <u>24</u>				
GEN. RATING	Orald		ļ			<del>                                     </del>				FAIR TO		1	<u> </u>		PERCHED	WATER,	SATURAT	TED ZONE	OR WATER BE	ARING S	STRATA	
AS A SUBGRADE	EX	CELLEN	IT TO GO	OOD		1	FAIR TO	POO	R	POOR	POOR	UNSUITABLE	HC_	_	HOLE CA	VE						
JODGICADE	Р	.I. OF	A-7-5	ا⊾≥	30	: P.I.	OF A-	-7-6	≱.l	L. – 30				<b>/-</b>	SPRING C	OR SEEPA	\GE					
			CON	ISIST	TENCY											MI	SCELL.	ANEOU	S SYMBOL	.S		
PRIMARY	SOIL TYPE	(	COMPACT				E OF S				of unconf ssive stre		9		WAY EMBANK			SPT DPT	OPT DMT TEST BO PMT	RING	SAMPLE	
		+	CONSIS		<u> </u>	(	(N-VALL	JE)		(1)	ONS/FT2)	1	Ų	WITH :	SOIL DESCRIF	PTION		•			DESIGNATIONS	
GENER GRANL			LOOS	Ε			<4 4 TO	10					l ⊥	- SOIL S	SYMBOL			$\oplus$	AUGER BORIN	G	S - BULK SAMPLE	
MATER	IAL		MEDIUM DENS		E		10 TO 3				N/A				CIAL FILL 01		٨N	$\rightarrow$	CORE BORING		SS - SPLIT SPOON	
(NON-	-COHESIVE)		VERY D			•	>50						l BU		WAY EMBANK			$\vee$			SAMPLE ST - SHELBY TUBE	
			VERY S	OFT			<2				<0.25			INFER	RED SOIL BO	DUNDARIE	S	<b>*</b> O	MONITORING \	WELL	SAMPLE	
GENER SILT-C			SOFT MEDIUM	STIFF	.		2 TO 4				.25 TO 0.5 0.5 TO 1	5	TISITE	INFER	RED ROCK LI	INE		Δ	PIEZOMETER		RS - ROCK SAMPLE	
MATER	IAL		STIFF	nee			8 TO 1			•	1 TO 2	2	TT744	ALLUV	1AL SOIL BO	UNDARY		Δ	INSTALLATION		RT - RECOMPACTED	
(COHE	SIVE)		VERY S	IIFF			>30				2 TO 4 >4		25/025	DIP/D	IP DIRECTION	N OF		$\bigcirc$	SLOPE INDICATION		TRIAXIAL SAMI CBR — CBR SAMPLE	PLE
			TE	XTU	IRE OF	R GR.	AIN S	SIZE					├━	ROĆK	STRUCTURES	S		$\overline{}$	SPT N-VALUE		CBR - CBR SAMPLE	
U.S. STD. S	IFVE SIZE			4	10	40		30	200	270			0	SOUND	ING ROD			$\cup$	SI I II VALOL	•		
OPENING (M				4.76	2.0	0.4		.25	0.07								A D	BREVIA	TIONS			
BOULDE	ER C	OBBLE		RAVEL	_	COAF			FINE		SILT	CLAY		40	ALICED DEEL	ICAI	AD	DICE VIP				
(BLDR.		(COB.)		(GR.)		SAN (CSE.			SANI (F. SI	, ,	(SL.)	(CL.)			AUGER REFU BORING TERM				PMT - PRE SD SAND			
	MM 305		75		2.0		(	0.25		0.05	0.005	i		CL	CLAY CONE PENE	TD A TION	TEST		SL. – SILT, SLI. – SLIG			
SIZE I	N. 12"		3"												- COARSE	IRAHON	IESI		TCR - TRIC		FUSAL	
			<u>MOISTI</u>		<u> </u>		<u>.ATIO</u>	<u>N O</u>	F T	ERMS			ļ		DYNAMIC P		ON TEST		7 - UNIT			
	MOISTURE : RBERG LIMI				ELD MOIS DESCRIPT			GUID	E FOR	FIELD MOIS	TURE DES	CRIPTION		e - \	OID RATIO				$\gamma_d$ - DRY W - MOIST			
					- SATURA	TED -		LISIIA	11 Y 11	QUID; VERY	WFT USU	IALLY		F F FOSS.	– FOSSILIFE	ROUS			W - MOISTO	JRE CON	HENI	
			_		(SAT.)					W THE GRO					<ul><li>FRACTURE</li><li>FRAGMEN</li></ul>				VST - VAN	E SHEAR	R TEST	
PLASTIC	+ Liqui	D LIMIT													- MEDIUM							
RANGE <					- WET -	- (W)				REQUIRES ( IMUM MOIS1					EQU	IPMEN	T USE	D ON	SUBJECT	PROJ	ECT	
(PI) <sub>PL</sub> L	+ PLAS	TIC LIN	IIT										DRILL UN	IITS:		ADV	ANCING T	OOLS:		н	AMMER TYPE:	
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					PLAS								🖂 сме	E-550x		$  \; \sqcup \;$	TUNGC	ARBIDE IN:	SERTS	Σ		
NONPLASTIC	•			PI	LASTICITY		(PI)			DRY STR			l 🗀 🚚				CASING	□ w/	ADVANCER			
LOW PLAST	ICITY				0-5 6-1	5				SLIGH	Т		L.J. CME	E-750			TRICONE		STEEL TEETH	⊢-;	HAND TOOLS:	
MED. PLAST					16-2 26 0	5 R MORI	F			MEDIU HIGH			POF	RTABLE H	HOIST		TRICONE		" TUNGCARB.		POST HOLE DIGGER	
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DECON	DTIONS VA	V INO:	IDE COL	ne nn				· /TAL	ı per	, YEL-BRN,	BILLE CO	AV)	⊠ от⊦	IER(	CME-45		OTHER _	2-1/4"	H.S.A.		SOUNDING ROD	
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	·																	,			OTHER	

# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL UNIT SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

		ROCK D	DESCRIPTION		TERMS AND DEFINITIONS		
HARD ROCK ROCK LINE	( IS NON-COASTAL PLAIN MA	ATERIAL THAT V	WHEN TESTED, WOULD YIELD SPT RE STAL PLAIN MATERIAL WOULD YIELD	ALLUYUM (ALLUY.) - SOILS WHICH HAVE BEEN TRANSPORTED BY WATER.			
SPT REFUSA	AL IS PENETRATION BY A SPI	LIT SPOON SAI	WPLER EQUAL TO OR LESS THAN O.	AQUIFER - A WATER BEARING FORMATION OR STRATA.			
IN NON-COA		TRANSITION BET	WEEN SOIL AND ROCK IS OFTEN REPR	RESENTED BY A ZONE	ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.		
	ERIALS ARE TYPICALLY DIVIDE	D AS FOLOWS:			ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS,		
WEATHERED ROCK (WR)	PER	N-COASTAL PL	AIN MATERIAL THAT YIELDS SPT N	VALUES > 100 BLOWS	OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, AS SHALE, SLATE, ETC.  ARTESIAN — GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL		
CRYSTALLINE	FINE	TO COARSE (	GRAIN IGNEOUS AND METAMORPHIC I REFUSAL IF TESTED. ROCK TYPE I		AT WHICH IS IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.		
ROCK (CR)	GNE	ISS, GABBRO,	SCHIST, ETC.		CALCAREOUS (CALC.) - SOILS WHICH CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.		
NON-CRYSTALI ROCK (NCR)	LINE SEDI	IMENTARY ROCI	GRAIN METAMORPHIC AND NON-COA K THAT WOULD YEILD SPT REFUSAL E, SLATE, SANDSTONE, ETC.		COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.		
COASTAL PLAIN SEDIMENTARY I (CP)	N COAS	STAL PLAIN SE	DIMENTS CEMENTED INTO ROCK, BUICK TYPE INCLUDES LIMESTONE, SAN	T MAY NOT YIELD NDSTONE, CEMENTED	CORE RECOVERY (REC.) — TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.		
(GF)	SHELL		THERING		DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.		
FRESH	ROCK FRESH, CRYSTALS BRI HAMMER IF CRYSTALLINE.	RIGHT, FEW JOIN	NTS MAY SHOW SLIGHT STAINING. RO	OCK RINGS UNDER	DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.		
VERY SLIGHT (V. SLI.)		PECIMEN FACE	, SOME JOINTS MAY SHOW THIN CLA SHINE BRIGHTLY. ROCK RINGS UNDI		<u>DIP DIRECTION (DIP AZIMUTH)</u> — THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.		
SLIGHT (SLI.)	ROCK GENERALLY FRESH, JO	OINTS STAINED	AND DISCOLORATION EXTENDS INTO Y. IN GRANITOID ROCKS SOME OCC		EAULT — A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.		
(30.)			CRYSTALLINE ROCKS RING UNDER HA		FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.		
MODERATE (MOD.)			SCOLORATION AND WEATHERING EFFI DULL AND DISCOLORED, SOME SHOP		ELOAT — ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.		
(			SHOWS SIGNIFICANT LOSS OF STRE		FLOOD PLAIN (F.P.) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY		
SEVERE	AND DISCOLORED AND A MA	AJORITY SHOW	R STAINED. IN GRANITOID ROCKS, KAOLINIZATION. ROCK SHOWS SEVE	ERE LOSS OF STRENGTH	THE STREAM. <u>ECRIMATION (FM.)</u> — A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN		
(MOD. SEV.)	AND CAN BE EXCAVATED WI IF TESTED. WOULD YIELD SE		ST'S PICK. ROCK GIVES "CLUNK" S	OUND WHEN STRUCK.	THE FIELD.  JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.		
SEVERE (SEV.)	IN STRENGTH TO STRONG SO	OIL. IN GRANI	R STAINED. ROCK FABRIC CLEAR A TOID ROCKS ALL FELDSPARS ARE K		LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.		
	EXTENT. SOME FRAGMENTS  IF TESTED. YIELDS SPT N V.				LENS — A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.		
VERY SEVERE			R STAINED. ROCK FABRIC ELEMENT	TO ADE DISCEDNIDIE DIT	MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN		
(V. SEV.)	THE MASS IS EFFECTIVELY F	REDUCED TO S	OIL STATUS, WITH ONLY FRAGMENTS	OF STRONG ROCK	SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.		
	REMAINING. SAPROLITE IS A VESTIGES OF THE ORIGINAL		F ROCK WEATHERED TO A DEGREE REMAIN. <i>IF TESTED, YIELDS SPT</i>		PERCHED WATER — WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.		
COMPLETE			OT DISCERNIBLE, OR DISCERNIBLE O		RESIDUAL SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.		
	SCATTERED CONCENTRATIONS		AY BE PRESENT AS DIKES OR STRIN		ROCK QUALITY DESIGNATION (R.Q.D.) - A MEASURE OF ROCK QUALITY DESCRIBED BY: TOTAL LENGTH OF		
	ALSO AN EXAMPLE.	BOOK	LIADDNIECC		ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.		
VEDY HADD	CANNOT BE SCRATCHED BY		HARDNESS  HARP PICK. BREAKING OF HAND SE	PECIMENS REQUIRES	SAPROLITE (SAP.) - RESIDUAL SOIL WHICH RETAINS THE RELIC STRUCTURE OR FABRIC OF THE		
VERY HARD	SEVERAL HARD BLOWS OF	THE GEOLOGIS			PARENT ROCK.  SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND		
HARD	TO DETACH HAND SPECIME	EN.			RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, WHICH HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS		
MODERATELY HARD			GOUGES OR GROOVES TO 0.25 INC GISTS PICK. HAND SPECIMENS CAN		SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.		
MEDIUM HARD		MALL CHIPS TO	HES DEEP BY FIRM PRESSURE OF KI PEICES 1 INCH MAXIMUM SIZE BY I		STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) — NUMBER OF BLOWS (N OR B.P.F.) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS LESS THAN 0.1 FOOT PENETRATION WITH 60 BLOWS.		
SOFT		INCHES IN SIZE	Y KNIFE OR PICK. CAN BE EXCAVA E BY MODERATE BLOWS OF A PICK SSURE.		STRATA CORE RECOVERY (SREC.) — TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.		
VERY SOFT	OR MORE IN THICKNESS CA		XCAVATED READILY WITH POINT OF BY FINGER PRESSURE. CAN BE S		STRATA ROCK QUALITY DESIGNATION (S.R.O.D.) — A MEASURE OF ROCK QUALITY DESCRIBED BY: 10TAL LENGTH OF ROCK SEGMENTS MITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE 10TAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.		
FR	FINGERNAIL. RACTURE SPACING	Т	BEDDIN	IG	TOPSOIL (I.S.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.		
TERM		IG	TERM	THICKNESS	DENICH MARK. DIV MAIL 040		
VERY WIDE			VERY THICKLY BEDDED	> 4 FEET	BENCH MARK: PK NAIL 242		
WIDE	3 TO 10 FEET		THICKLY BEDDED THINLY BEDDED	1.5 - 4 FEET 0.16 - 1.5 FEET	ELEVATION: 648.77'		
MODERATE CLOSE	ELY CLOSE 1 TO 3 FEET 0.16 TO 1 FEE	<sub>FT</sub>	VERY THINLY BEDDED	0.03 - 0.16 FEET			
VERY CLOS			THICKLY LAMINATED THINLY LAMINATED	0.008 - 0.03 FEET < 0.008 FEET	NOTES:		
		INDÙ	RATION				
FOR SEDIMENTA	ARY ROCKS, INDURATION IS T	THE HARDENING	OF THE MATERIAL BY CEMENTING,	HEAT, PRESSURE, ETC.			
FRI	IABLE		WITH FINGER FREES NUMEROUS GRAI OW BY HAMMER DISINTEGRATES SAI				
мог	DERATELY INDURATED		NN BE SEPARATED FROM SAMPLE W ASILY WHEN HIT WITH HAMMER.	TH STEEL PROBE;			
IND	DURATED		RE DIFFICULT TO SEPARATE WITH ST TO BREAK WITH HAMMER.	TEEL PROBE;			
1							

SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

EXTREMELY INDURATED



DRAWN BY:

MBL

CHECKED BY:

DDB

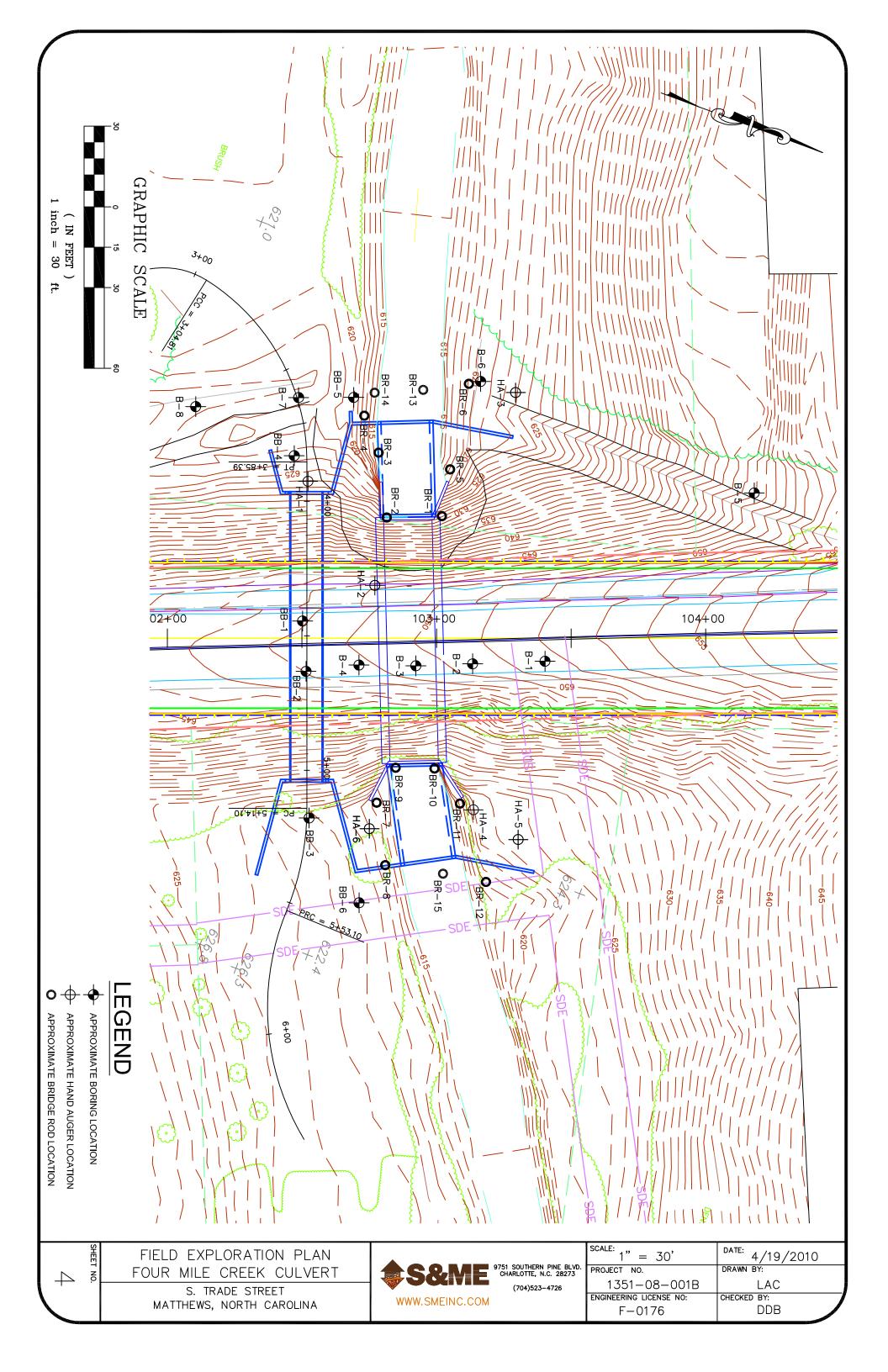
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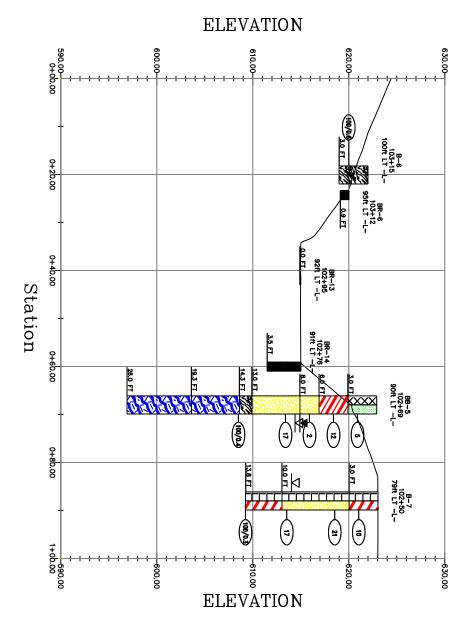


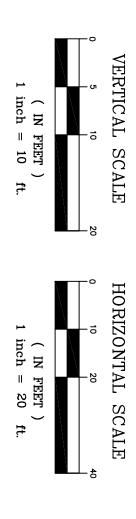
### FOUR MILE CREEK CULVERT

S TRADE STREET MATTHEWS, NORTH CAROLINA

JOB NO.: 1351-08-001B







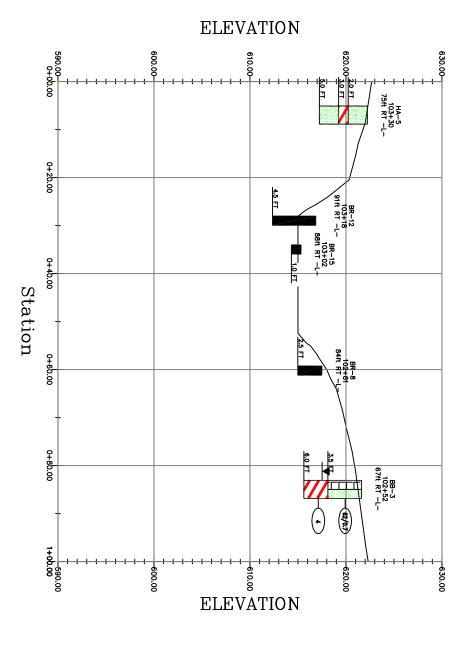
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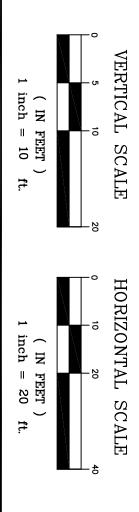
95 FEET LT -L-

S TRADE STREET ROADWAY WIDENING MATTHEWS, NORTH CAROLINA



SCALE: AS SHOWN	DATE: 4/19/2010
PROJECT NO.	DRAWN BY:
1351-08-001B	CD
ENGINEERING LICENSE NO:	CHECKED BY:
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GENERALIZED SUBSURFACE PROFILE

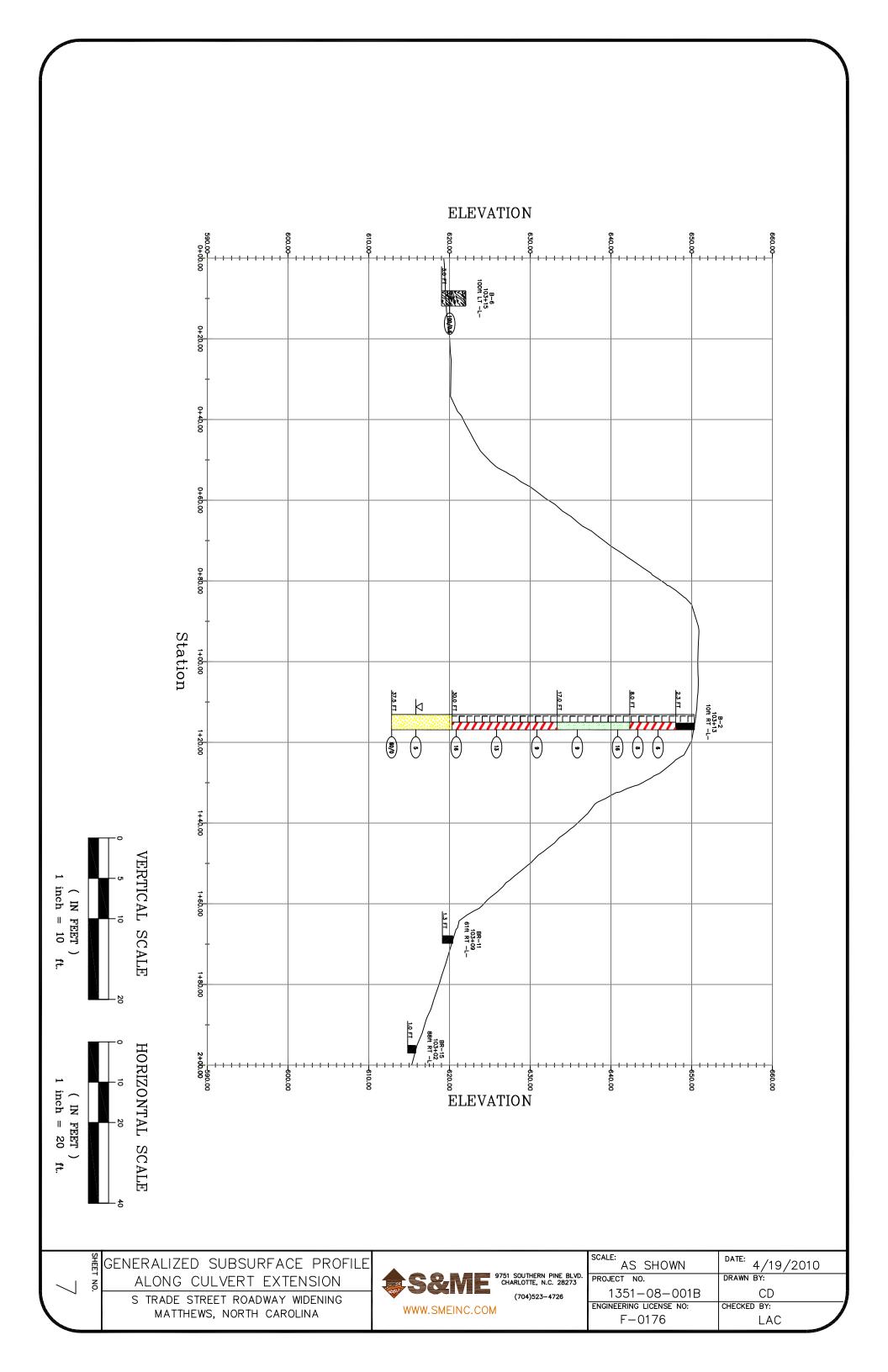
80 FEET RT -L
S TRADE STREET ROADWAY WIDENING

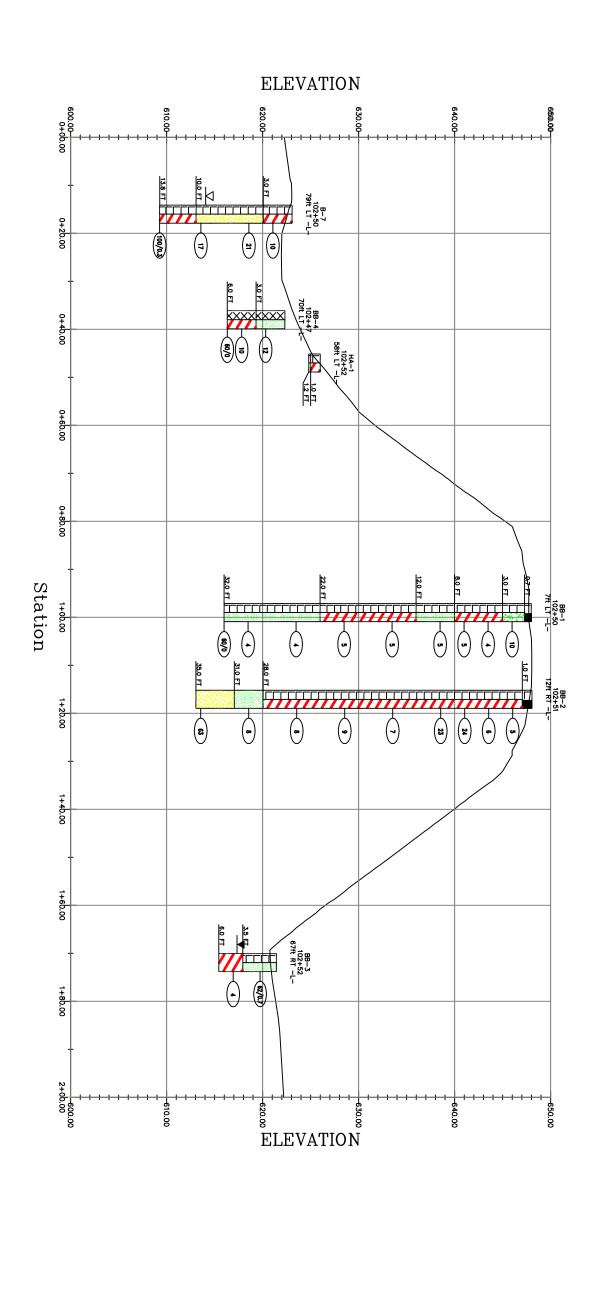
MATTHEWS, NORTH CAROLINA

9751 SOUTHERN PINE BLVD. CHARLOTTE, N.C. 28273 (704)523–4726

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( IN inch

FEET = 20

( IN FEET inch = 10

VERTICAL SCALE

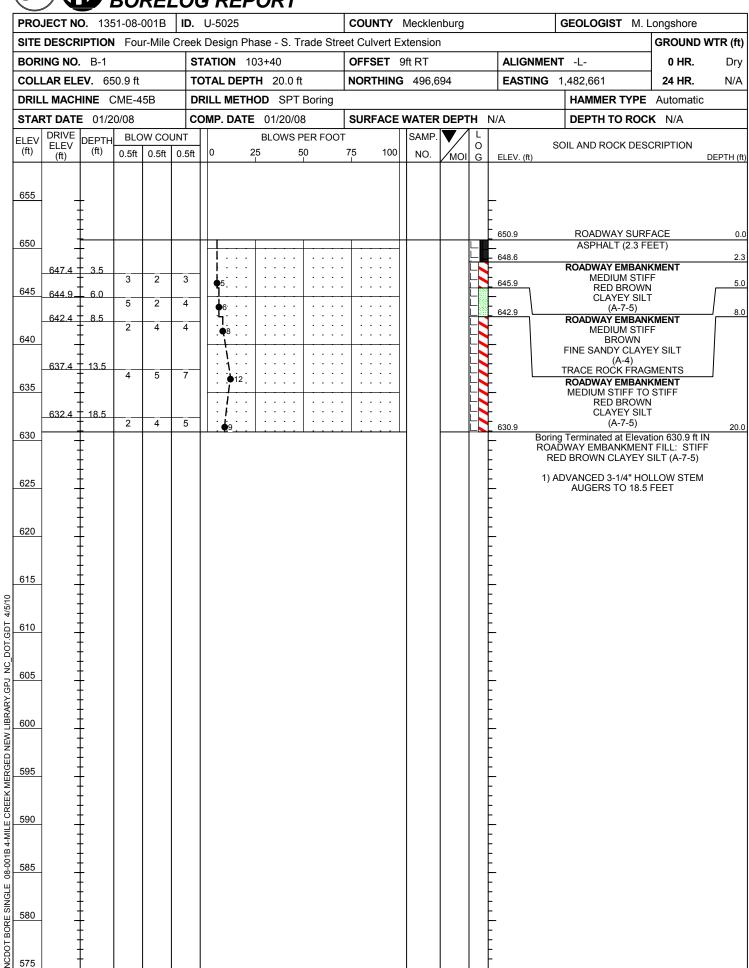
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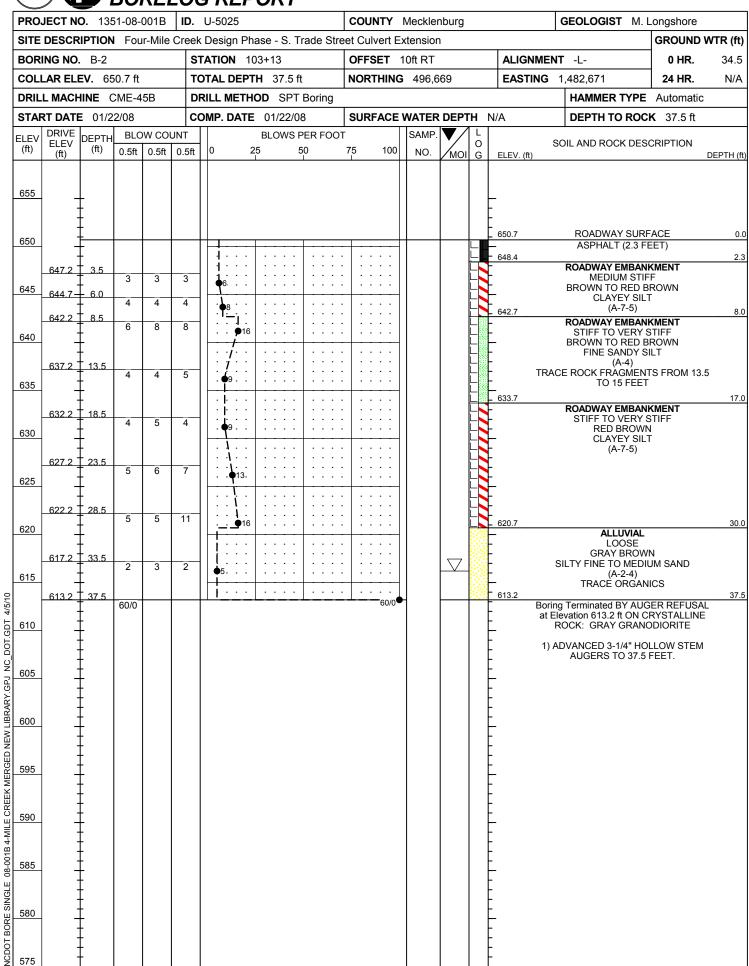
GENERALIZED SUBSURFACE PROFILE
ALONG PEDESTRIAN TUNNEL

S TRADE STREET ROADWAY WIDENING MATTHEWS, NORTH CAROLINA

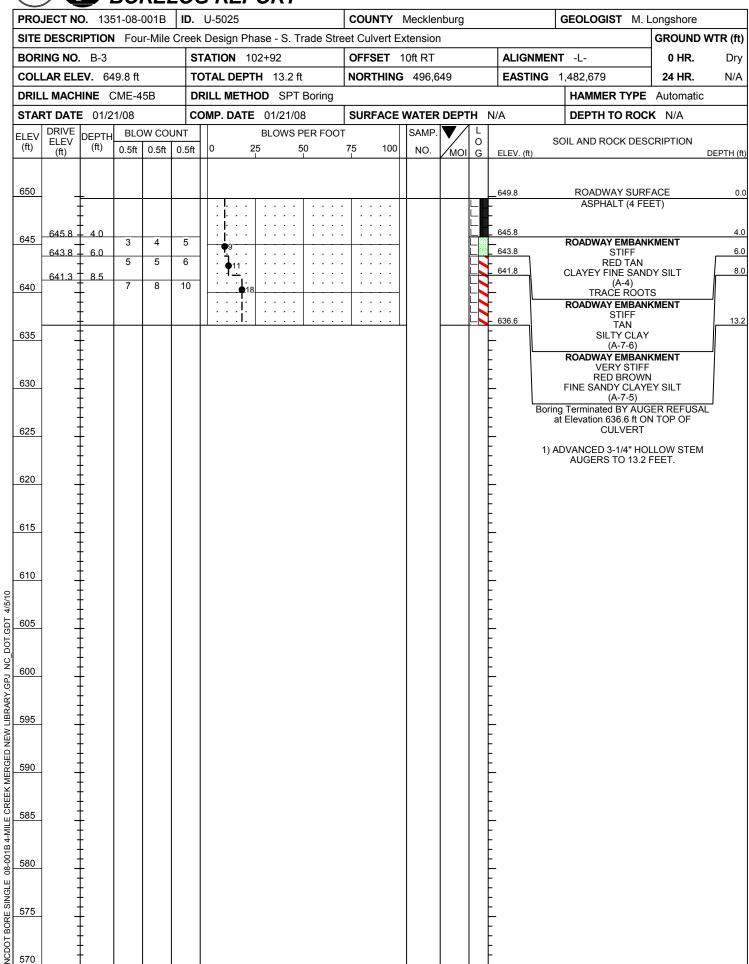


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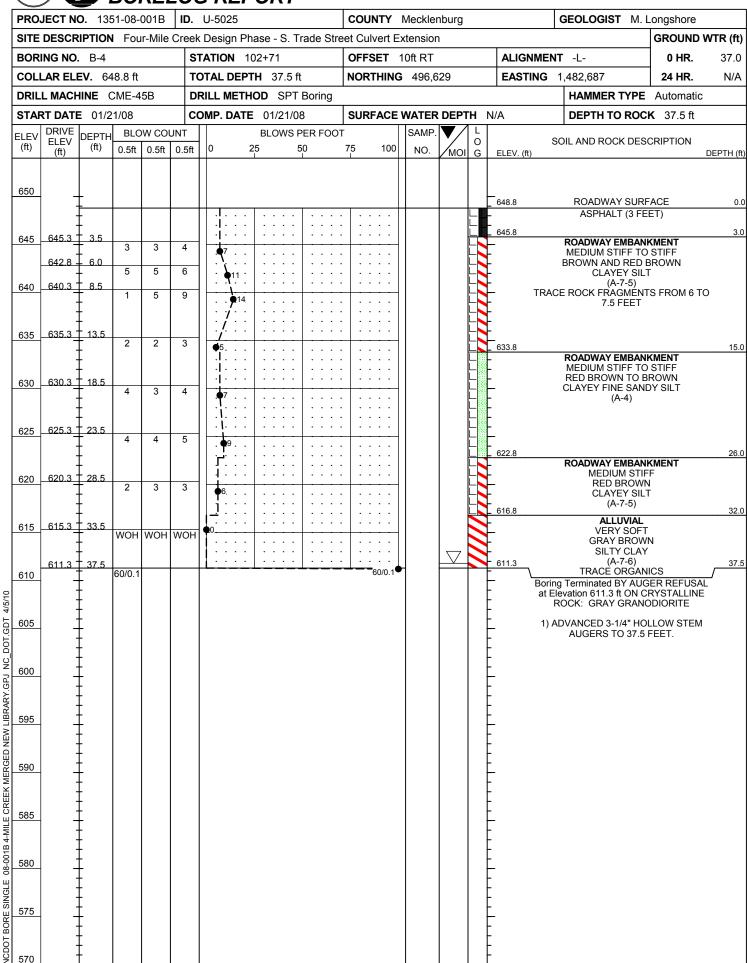
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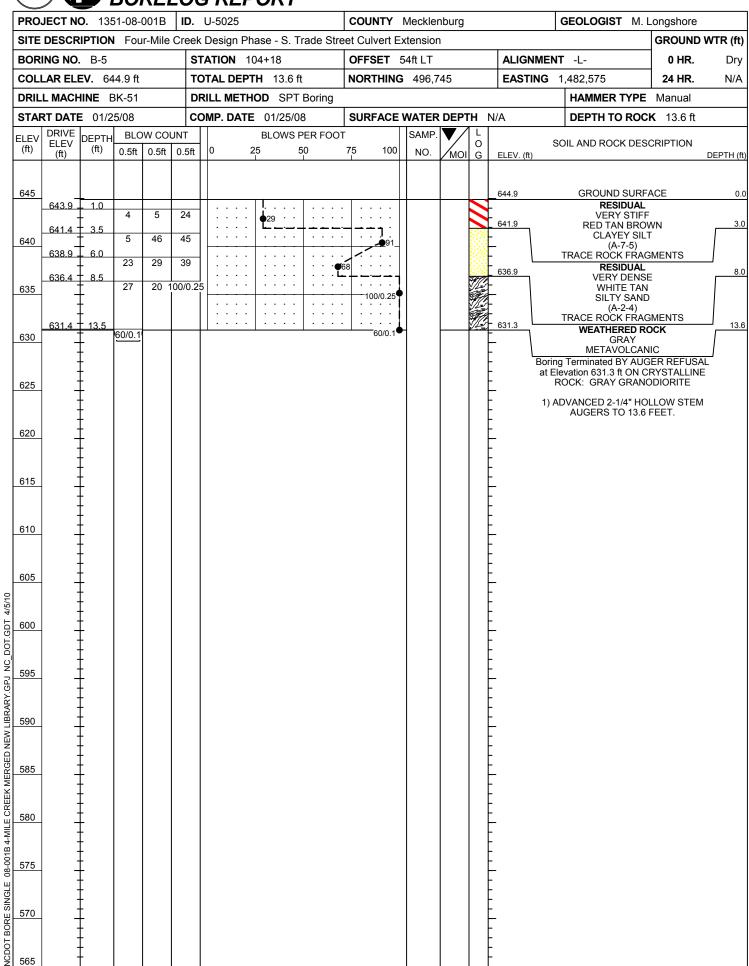


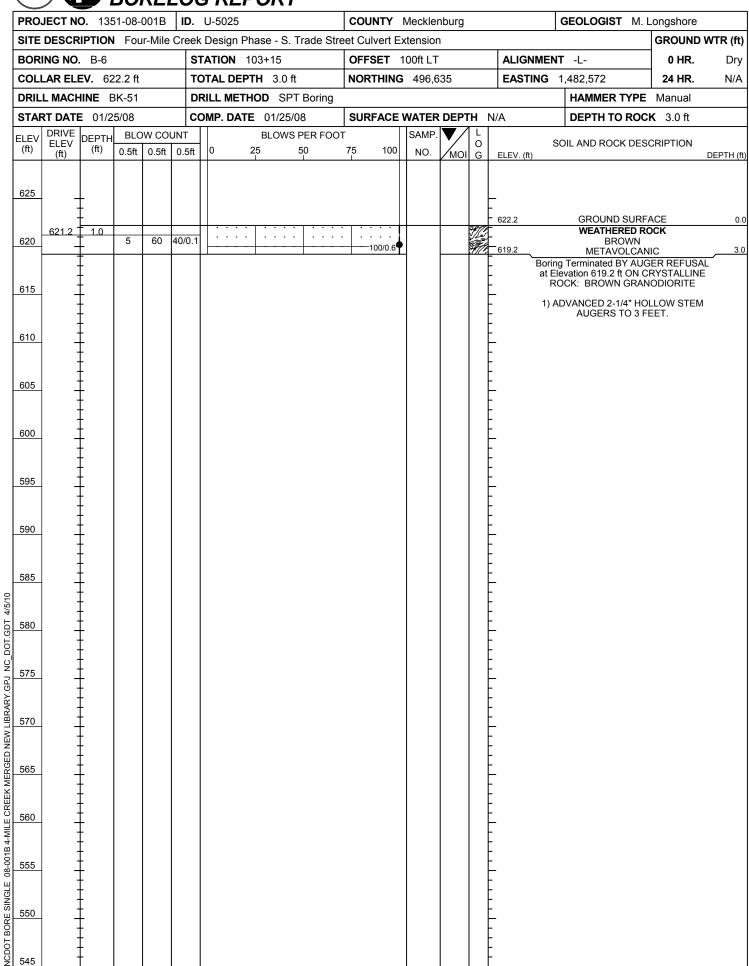
DOT.GDT

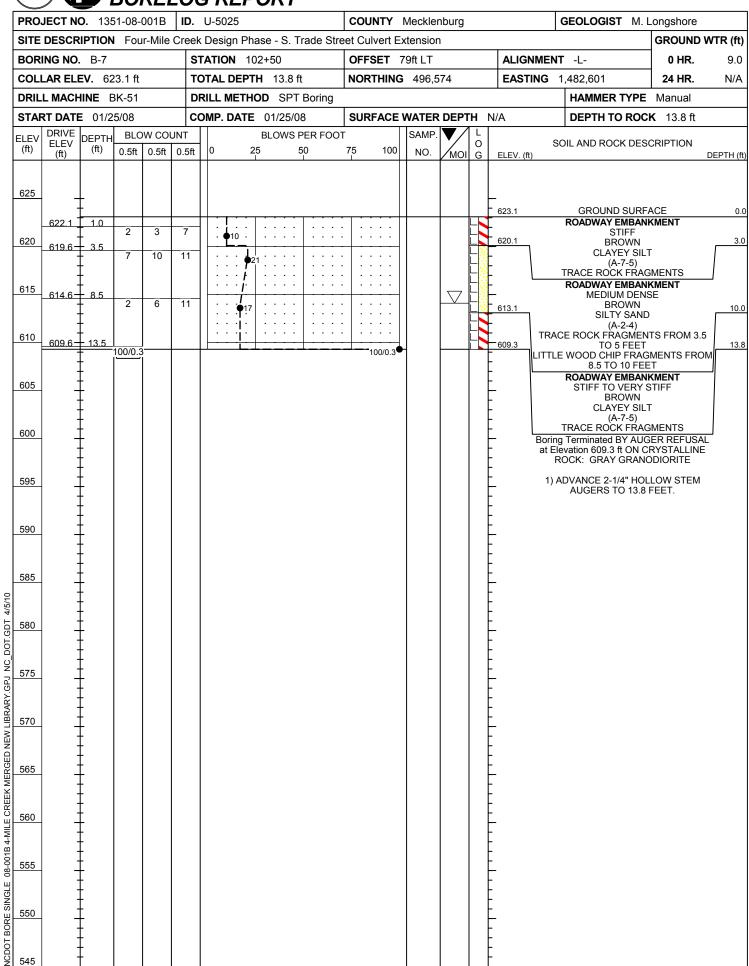
08-001B 4-MILE CREEK MERGED NEW LIBRARY.GPJ NC

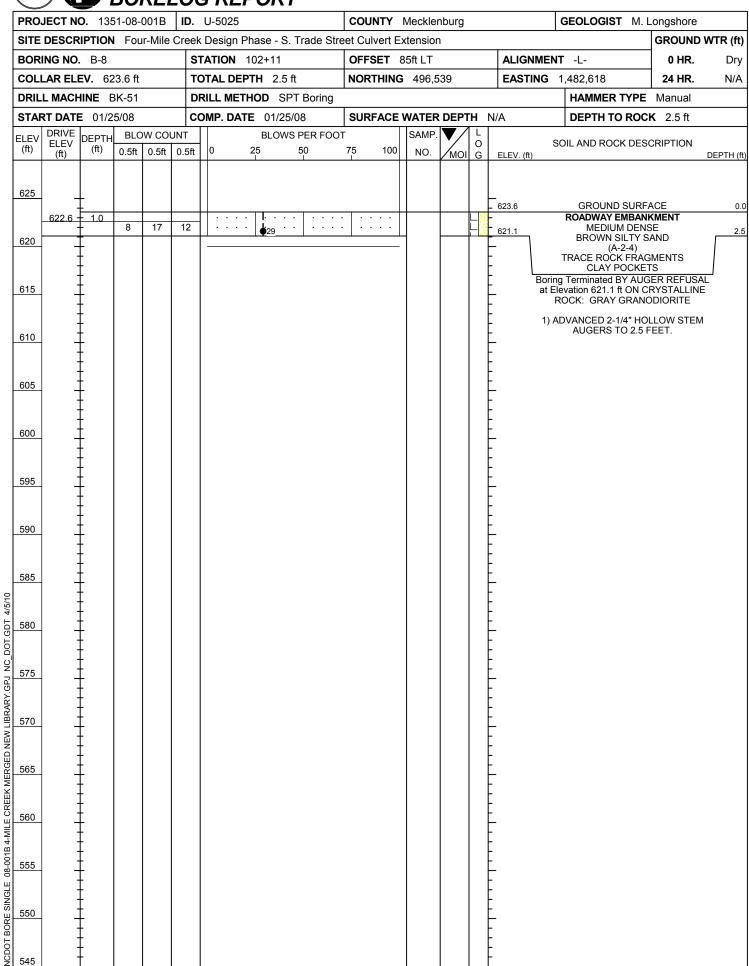
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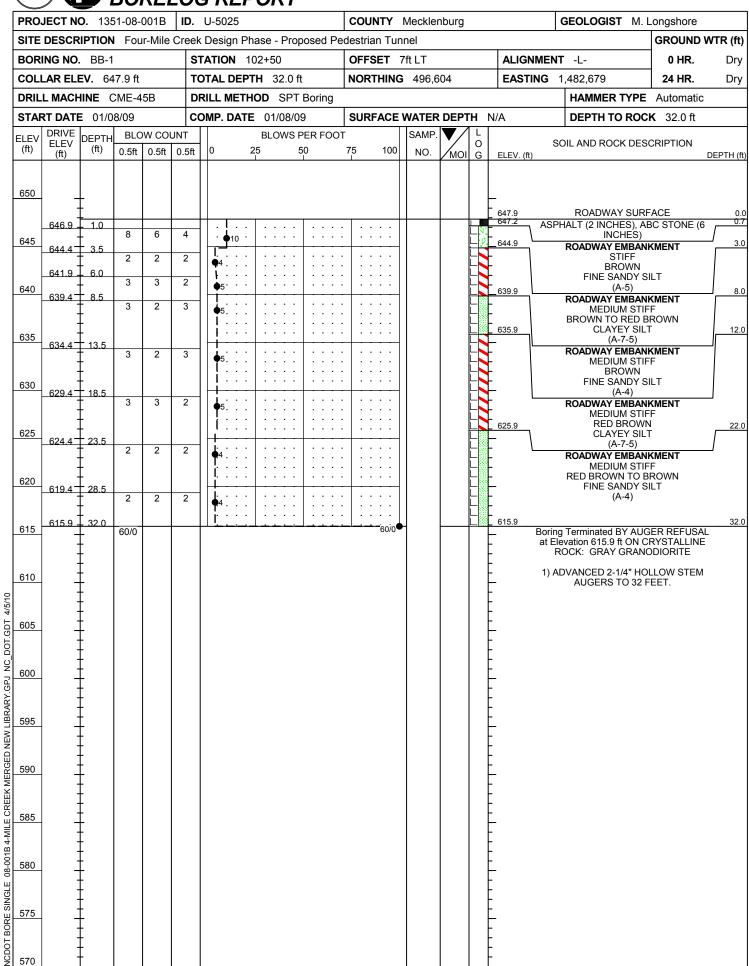


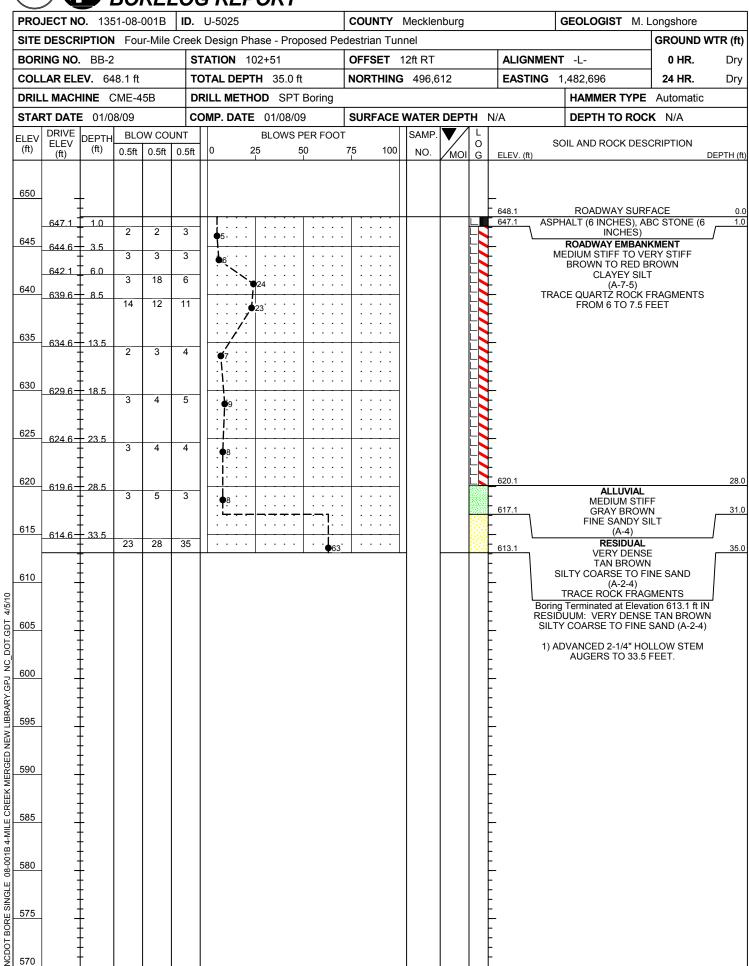


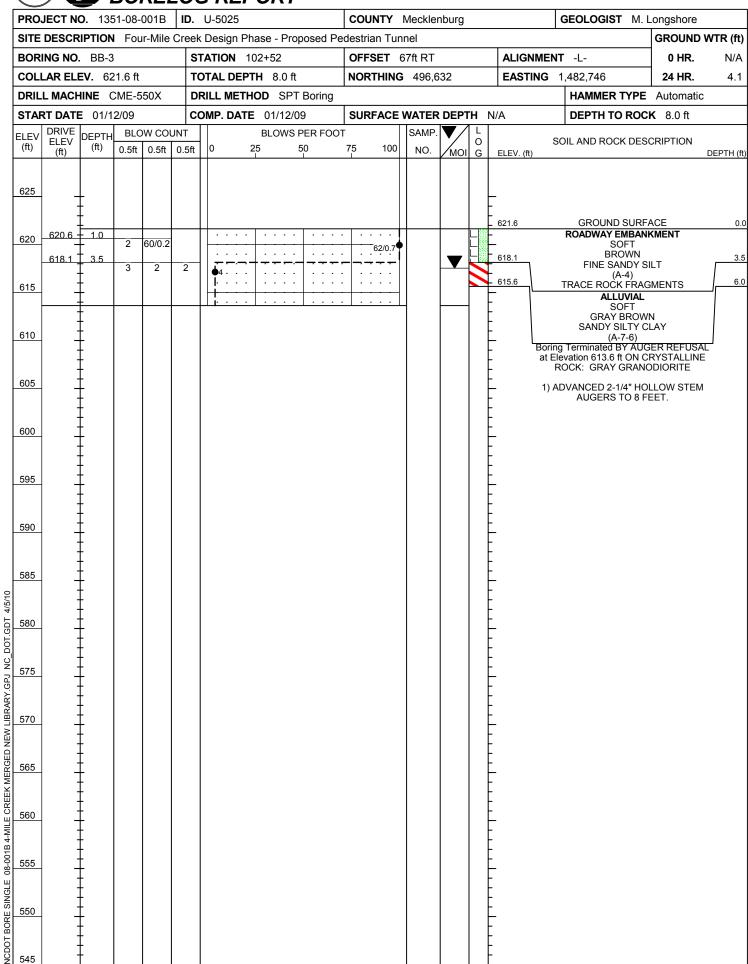


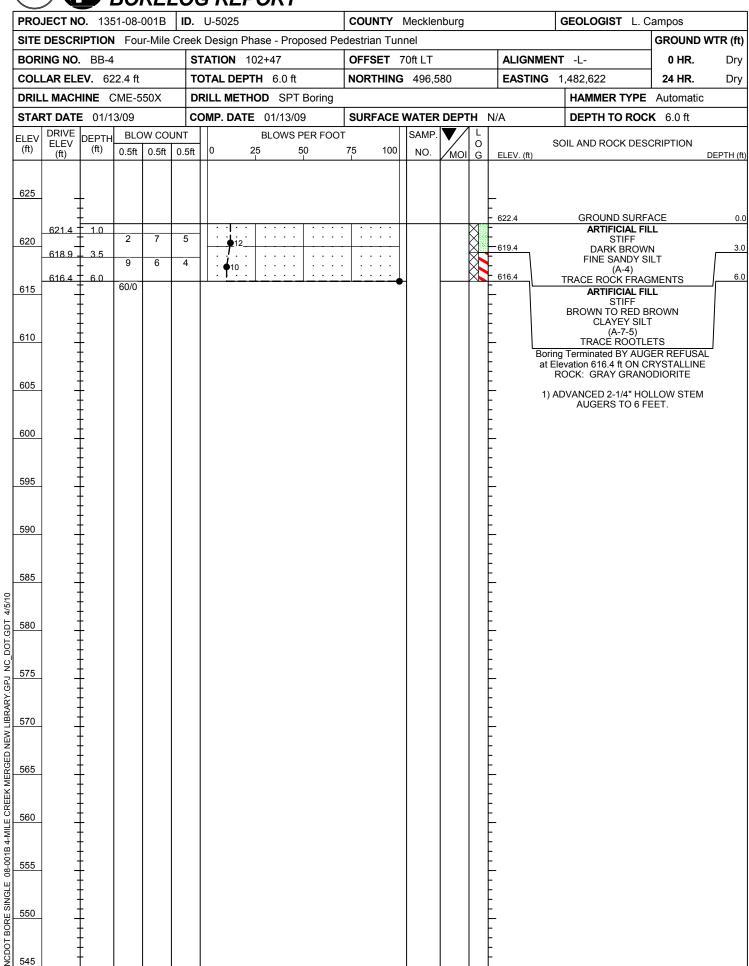


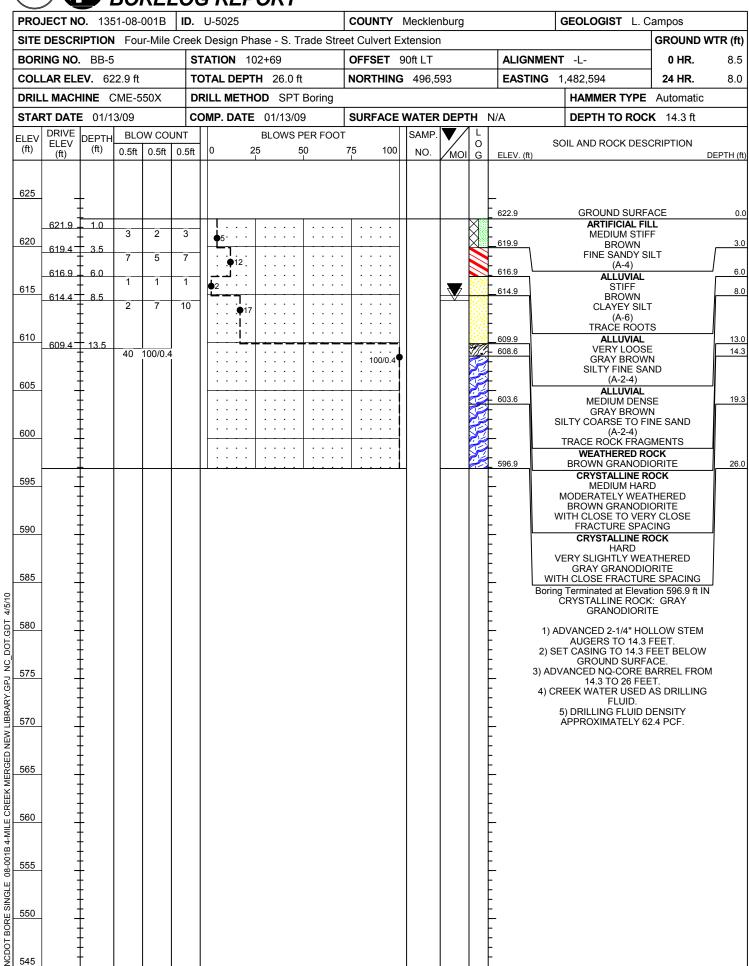


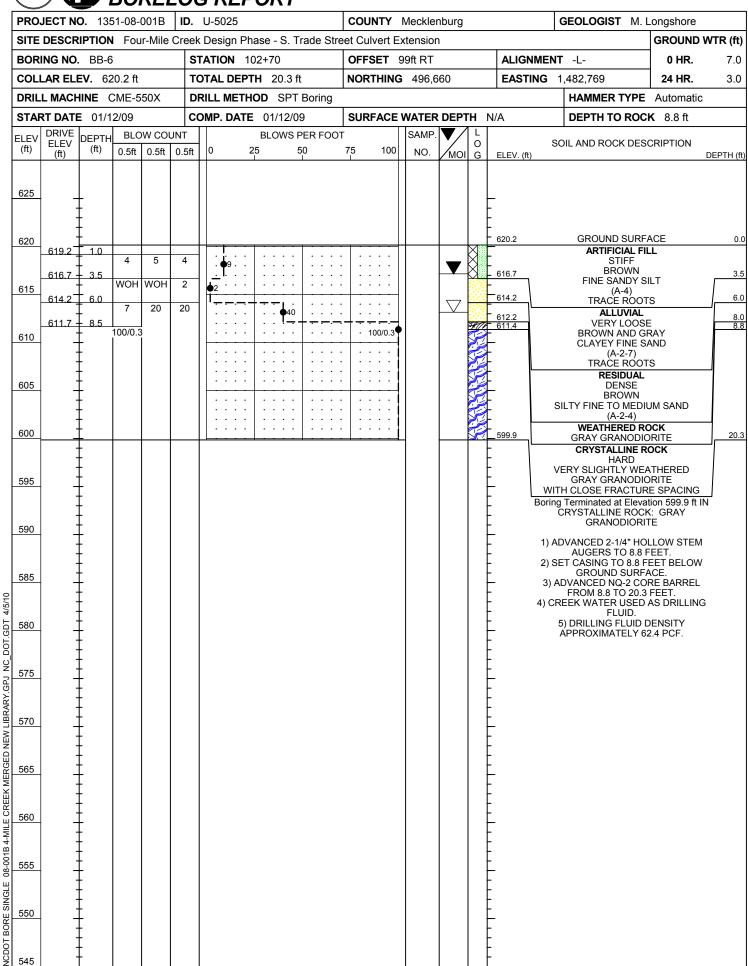












PRO.	JECT N	<b>O.</b> 13	51-08-0	001B I	<b>D.</b> U-	5025				CC	UNTY	Mecklenburg		GEOLOGIST L. C	Campos	
SITE	DESCR	IPTIO	<b>I</b> Fou	ır-Mile Cr	eek D	esign I	Phase - S	S. Trac	le Stre	eet C	ulvert Ex	tension	•		GROUND V	VTR (ft
BORI	NG NO	. BB-	5		STA	ΓΙΟΝ	102+69			OF	FSET 9	Oft LT	ALIGNMEN	T -L-	0 HR.	8.5
COLL	AR ELI	<b>EV</b> . 6	22.9 ft		тот	AL DE	<b>PTH</b> 26	.0 ft		NO	RTHING	496,593	EASTING	1,482,594	24 HR.	8.0
DRILI	L MACH	IINE (	CME-5	50X	DRIL	L ME1	THOD S	PT Bo	ring					HAMMER TYPE	Automatic	
STAR	RT DATE	E 01/1	3/09		СОМ	P. DA	<b>TE</b> 01/1	3/09		SU	RFACE \	WATER DEPTH N	/A	DEPTH TO ROC	<b>K</b> 14.3 ft	
CORE	SIZE	NQ-2					<b>N</b> 11.7 f			DR	ILLER	J. LITTLE				
(ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	REC. (ft) %	JN RQD (ft) %	SAMP. NO.	STR REC. (ft) %	ATA RQD (ft) %	L O G	ELEV. (ft		ESCRIPTION A	ND REMARKS	I	DEPTH (
08.58	608.6	143	4.7		(0.0)	(0.0)		(2.0)	(0.5)		000.0		Begin Coring			14
-	608.6 - 606.9 _	<u> 16.0</u>	1.7 5.0		(0.9)	(0.0)		(3.8) 76%	(0.5) 10%		- 608.6 -		MEDIUN			14
605	-	E			(4.8) 96%	(2.2) 44%					 - 603.6		BROWN GRA	WEATHERED  NODIORITE	ACINO	19
	601.9	21.0						(6.7) 100%	(5.5)		-	WITH CLOS	JOINTS INDI		ACING	<u></u>
600	_		5.0		(5.0) 100%	(4.1) 82%		100%	02 /0		-		HA			
	-	<u> </u>									-		GRAY GRA			
	596.9	26.0									_ 596.9			ACTURE SPACING NT AT 30°, 1 JOINT A	AT 65°	26
595	_	Ĺ									_	Boring Terminated at	Elevation 596.9	ft IN CRYSTALLINE DIORITE	ROCK: GRA	₹′
	-	<u> </u>									-	1) ADVANCED 2		STEM AUGERS TO	1/1 3 FEET	
590	_	‡									_	2) SET CASING	TO 14.3 FEET	BELOW GROUND S RREL FROM 14.3 TO	SURFACE.	
	-	‡									<b>-</b>	4) CREE	K WATER USE	D AS DRILLING FLU APPROXIMATELY 6	IID.	
E0E	-	-									-	5) DRILLING F	LOID DENSIT I	APPROXIMATELT	)2.4 PGF.	
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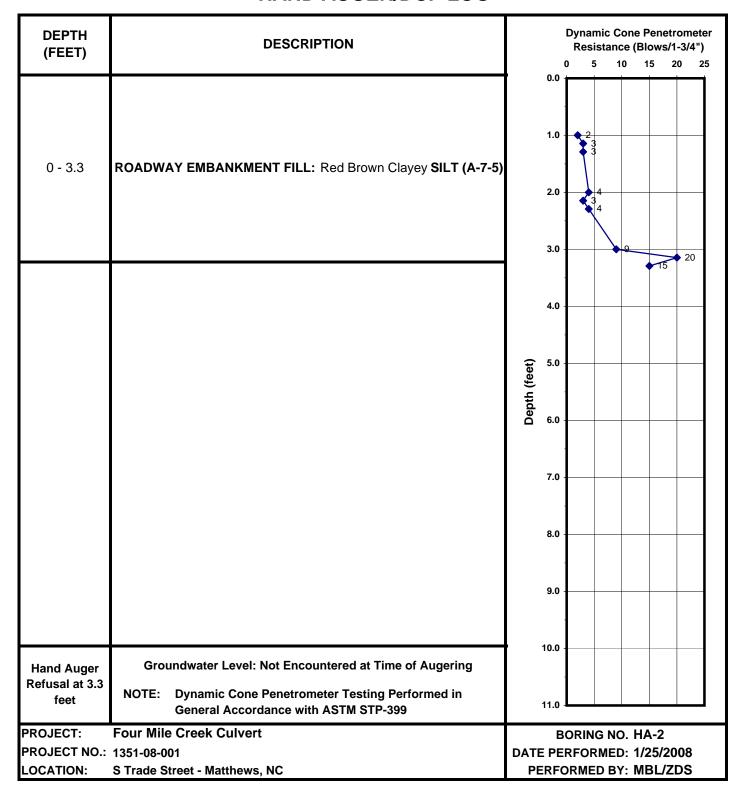


PRO.	JECT N	<b>O</b> . 13	51-08-	001B   I	<b>D</b> . U-	5025				CC	OUNTY Meck	enburg		GEOLOGIST M. I	Longshore	
SITE	DESCR	IPTIO	<b>I</b> Fou	ır-Mile Cr	eek D	esign l	Phase - S	S. Trac	le Stre	eet C	Culvert Extensi	on			GROUND W	TR (ft)
BORI	NG NO	. BB-6	3		STAT	TION	102+70			OF	FSET 99ft R	Γ	ALIGNMEN	IT -L-	0 HR.	7.0
COLL	AR ELI	<b>EV</b> . 6	20.2 ft		тот	AL DE	<b>PTH</b> 20	.3 ft		NO	RTHING 496	,660	EASTING	1,482,769	24 HR.	3.0
DRIL	L MACH	IINE	CME-5	550X	DRIL	L ME	THOD S	PT Bo	ring	•				HAMMER TYPE	Automatic	
STAR	RT DATI	<b>=</b> 01/	12/09		сом	P. DA	<b>TE</b> 01/1	2/09		su	RFACE WATE	R DEPTH N/	'A	DEPTH TO ROC	<b>K</b> 8.8 ft	
COR	SIZE	NQ-2			TOTA	AL RU	<b>N</b> 11.5 f	t		DR	RILLER J. LIT	TLE		-		
ELEV	RUN ELEV	DEPTH		DRILL RATE	REC.	RQD	SAMP.	REC.	ATA RQD	L		DE	ESCRIPTION A	AND REMARKS		
(ft)	(ft)	(ft)	(ft)	(Min/ft)	(ft) %	(ft) %	NO.	(ft) %	(ft) %	Ğ	ELEV. (ft)		_SCRIFTION /	AND KEWAKKS	D	EPTH (fi
11.36	611.4		ļ. <u>.</u>		(4.5)	(4.4)		(44.5)	(0.0)				Begin Corir			
610	611.4 609.9	10.3	1.5 5.0			(1.1) 73%		100%	(8.0) 70%		611.4		HA	LINE ROCK ARD		8.8
		F	0.0		(5.0) 100%	(2.2) 44%					F		GRAY GRA	_Y WEATHERED ANODIORITE		
605	604.9_	[ _ 15.3									[ 8、			ACTURE SPACING AT 20°-40°, 6 JOINTS	S AT 50°-65°	
	-		5.0		(5.0) 100%	(3.1)					F					
		F			10070	0270					F					
600	599.9	20.3	-								599.9 Borin	n Terminated at	Flevation 500	9 ft IN CRYSTALLINE	ROCK GRAY	20.
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595	-	Ŧ												V STEM AUGERS TO		
	-	F									F 3	) ADVANCED N	Q-2 CORE BA	BELOW GROUND SI	20.3 FEET.	
		ļ									-	4) CREE 5) DRILLING FI	K WATER USI LUID DENSIT	ED AS DRILLING FLU Y APPROXIMATELY 6	11D. 32.4 PCF.	
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DEPTH (FEET)	DESCRIPTION		Dynamic Cone Penetrometer Resistance (Blows/1-3/4")
0 - 1.0	ROADWAY EMBANKMENT FILL: Red Brown Clayey SILT (A-7-5)		0 5 10 15 20 25
1.0 - 1.2	ROADWAY EMBANKMENT FILL: Red Brown Fine Sandy SILT (A-4)		1.0 7 9 12
			2.0
			3.0
			4.0
		Depth (feet)	5.0
		Depth	6.0
			7.0
			8.0
			9.0
Hand Auger	Groundwater Level: Not Encountered at Time of Augering	1	0.0
Refusal at 1.2 feet	NOTE: Dynamic Cone Penetrometer Testing Performed in General Accordance with ASTM STP-399	1	11.0
PROJECT: PROJECT NO.: LOCATION:	Four Mile Creek Culvert 1351-08-001 S Trade Street - Matthews, NC		BORING NO. HA-1 PERFORMED: 1/25/2008 RFORMED BY: MBL/ZDS





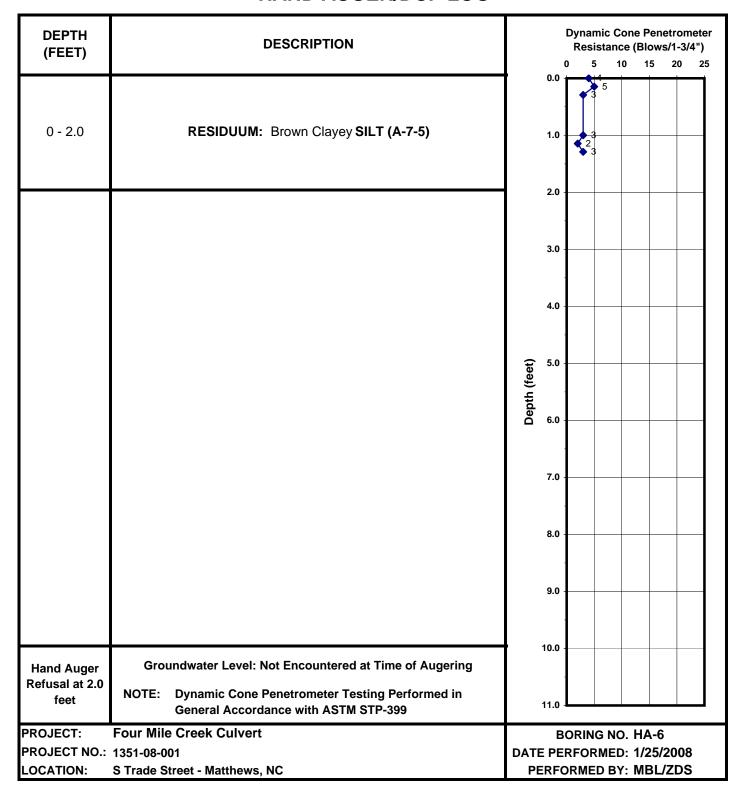


DEPTH (FEET)	DESCRIPTION		Dynamic Cone Penetrometer Resistance (Blows/1-3/4") 0 5 10 15 20 25
0 - 1.0	RESIDUUM: Brown Fine Sandy SILT (A-4)		0.0
1.0 - 2.0	Red Brown Clayey <b>SILT (A-7-5)</b> with rock fragments and pockets of highly plastic clay		1.0 3 5
2.0 - 3.0	Red Brown and Gray Silty CLAY (A-7-6)		3.0
			4.0
		et)	5.0
		Depth (feet)	6.0
			7.0
			8.0
			9.0
Hand Auger	Groundwater Level: Not Encountered at Time of Augering		10.0
Refusal at 3 feet	NOTE: Dynamic Cone Penetrometer Testing Performed in General Accordance with ASTM STP-399		11.0
PROJECT: PROJECT NO.: LOCATION:	Four Mile Creek Culvert 1351-08-001 S Trade Street - Matthews, NC		BORING NO. HA-4 E PERFORMED: 1/25/2008 ERFORMED BY: MBL/ZDS



DEPTH (FEET)	DESCRIPTION		Dynamic Cone Penetrometer Resistance (Blows/1-3/4") 0 5 10 15 20 25
0 - 2.0	RESIDUUM: Brown Fine Sandy SILT (A-4)		1.0
2.0 - 3.0	Brown Clayey <b>SILT (A-7-5)</b>		2.0
3.0 - 4.0	Brown Clayey Fine Sandy <b>SILT (A-4)</b> (saturated)		3.0 4 4 6 6 4.0
4.0 - 5.0	Tan Fine Sandy <b>SILT (A-4)</b> with rock fragments	٠	5.0
Hand Auger Refusal at 5	Groundwater Level: Not Encountered at Time of Augering NOTE: Dynamic Cone Penetrometer Testing Performed in	Depth (feet)	6.0
feet	General Accordance with ASTM STP-399		11.0
PROJECT: PROJECT NO.: LOCATION:	Four Mile Creek Culvert 1351-08-001 S Trade Street - Matthews, NC		BORING NO. HA-5 E PERFORMED: 1/25/2008 ERFORMED BY: MBL/ZDS





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PROJECT		351-08-	001B	ID (	J-520	)5	71.		co Meckleni		11/	GEO	M. Longshore		
NUMBER SITE		ide Stre		.1			 Y								
BORING		R-1		STA	VVIG	21 111 15	2		OFFSET	FT		ALIGN			
NUMBER ELEVATION			FT	TOTAL				FΥ	NORTH			MENT			
DRILL.				DEPTH				F1	<u> </u>			DRILL	ER M Langahara		
METHOD START		ridge R	oa 	COMP		4 10 5	·00		SURFACE			DEPT	W. Longshore		
DATE	01/2			DATE		1/25		-	WTR DEPTH	71	FT	TO RO	рск Г'	V DESCRIPTION	
DEPTH (ft)	0.5 ft	BLOW COU 0,5 ft	TOTAL	0	25 25	50 50	R FOO	1 75 10	SAMPLE NO. 8 INTERVAL	моі	ORI	GIN	SOIL & ROC SOIL or ROCK NAME (w/ color, density/o	K DESCRIPTION consistency, texture, plasticity,	organics, other)
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SHEET 30 OF 51

NCDOT GEOTECHNICAL ENGINEERING UNIT

IUMBER	1351-08-001B	" L	U-5205	Mecklenb	urg		GEO	M. Longshore	
ITE ESC	S. Trade Street Roa	adway	Widening						
ORING	BR-3	STA		OFFSET	FT		ALIGN-		
IUMBER LEVATION		TOTAL		NORTH			MENT EAST		
		DEPTH	FT				DRILLE		
RILL IETHOD	Bridge Rod						i	W. Longshore	
TART DATE	01/25/08	COMP	01/25/08	SURFACE WTR DEPTH		FT	DEPTH TO RO	ck FT	
DEPTH	BLOW COUNT		BLOWS PER FOOT	SAMPLE NO.	T			SOIL & R	OCK DESCRIPTION
(ft)	0.5 ft 0.5 ft TOTAL	0	25 50 75 100	& INTERVAL	MOI	OR	IGIN	SOIL or ROCK NAME (w/ color, den	sity/consistency, texture, plasticity, organics, other)
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RED LINE DECK TO DATUM DISTANCE Form GEU-005e

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PROJECT NUMBER	1351-08-001B	U-5205	co Mecklenburg	GEO	M. Longshore	
SITE DESC	S. Trade Street Ro			<u>-</u>		
BORING NUMBER	BR-6	STA	OFFSET FT	ALIGN- MENT	•	
ELEVATIO	E1	TOTAL FT DEPTH	NORTH	EAST		
DRILL METHOD START	Bridge Rod	COMP 01/25/09	SURFACE	DRILLE ET DEPTH	W. Longshore	
DATE	01/25/08 BLOW COUNT	DATE 01/25/08 BLOWS PER FOOT	WTR DEPTH SAMPLE NO.	FT TO RO	ск	K DESCRIPTION
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TH		LOW COU	INT	DAT	E				R FO	TC			SAMPLE NO.	-!		101	RUCK	S		DESCRIPTION	
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PROJECT NUMBER	1351-08-001B	<sup>ID</sup> U-5205	co Mecklen		GEO M. Longshore	
SITE DESC	S. Trade Street Roa	adway Widening				
BORING NUMBER	BR-9	STA	OFFSET	FT	ALIGN- MENT	
ELEVATION	N FT	TOTAL DEPTH	FT NORTH		EAST	
DRILL METHOD	Bridge Rod	•			DRILLER M. Longshore	
START DATE	01/25/08	COMP DATE 01/25/08	SURFACE WTR DEPTH	FΥ	DEPTH FT FT	
DEPTH (ft)	BLOW COUNT 0.5 ft 0.5 ft TOTAL	BLOWS PER FOC 0 25 50	T SAMPLE NO. 75 100 & INTERVAL	MOI ORIG	SOIL or ROCK NAME (w/ color, dens	OCK DESCRIPTION ity/consistency, texture, plasticity, organics, other)
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SITE DESC	S. Trad	le Stre	et Roa	adwa	ay W	/ider	ning						•	J		
BORING NUMBER		₹-11		STA							OFFSET	FT		ALIGN MENT		
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DATE	01/25	/08 ow.cour	NIT	DATE			/25/(	)8 R FOO			WTR DEPTH SAMPLE NO.	···	FT	TO RC	ск	DESCRIPTION
DEPTH (ft)	0.5 ft	0.5 ft	TOTAL	0	25		50			100	& INTERVAL	моі	ORIG	SIN		onsistency, texture, plasticity, organics, other)
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BR-1 Bridge 01/25/08 BLOW	e Rod COUNT	T TOTAL DEPTH	L H	01/2 BLOWS	/25/ 'S PE	/08 ER FOO			NORTH SURFACE WIR DEPTH SAMPLE NO.			MENT EAST DRILLER DEPTH	rk FT
Bridge 01/25/08 BLOW	e Rod 3 count	T TOTAL DEPTH	H 	BLOWS	S PE	R FOO			NORTH SURFACE WIR DEPTH SAMPLE NO.			MENT EAST DRILLER DEPTH	rk FT
01/25/08 BLOW	e Rod 3 COUNT	COMP DATE	H 	BLOWS	S PE	R FOO			SURFACE WTR DEPTH SAMPLE NO.	MOI		DRILLEF	rk FT
01/25/08 BLOW	COUNT	COMP DATE	E	BLOWS	S PE	R FOO		100	SAMPLE NO.	MOI		DEPTH	rk FT
01/25/08 BLOW	COUNT	DATE	E	BLOWS	S PE	R FOO		100	SAMPLE NO.	MOI		DEPTH TO ROC	ск гі
BLOW	COUNT		E	BLOWS	S PE	R FOO		100	SAMPLE NO.	MOI		1	
0.5 ft 0.	5.6 TO	AL 0	25	5	50		75	100	& INTERVAL	· MOI	1 ~~	ICIN'	SOIL & ROCK DESCRIPTION
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RED DECK TO DATUM DISTANCE FT Form GEU-005e Revised 2/6/2007



Core B-5



Core B-6



### Photograph No. 1:

This photograph was taken from the south creek bank on the west side of Trade Street looking north along the end of the proposed culvert extension.



#### Photograph No. 2:

This photograph was taken from the south creek bank on the west side of Trade Street looking upstream.



#### Photograph No. 3:

This photograph was taken from the south creek bank on the west side of Trade Street looking downstream.



### Photograph No. 4:

This photograph was taken from the north creek bank on the west side of Trade Street looking south along the end of the proposed culvert extension.



### Photograph No. 5:

This photograph was taken from the south creek bank on the east side of Trade Street looking downstream.



## Photograph No. 6:

This photograph was taken from the south creek bank on the east side of Trade Street looking upstream.



#### Photograph No. 7:

This photograph was taken from the south creek bank on the east side of Trade Street looking north along the end of the proposed culvert extension.



#### Photograph No. 8:

This photograph was taken from the north creek bank on the east side of Trade Street looking south along the end of the proposed culvert extension.



## FIELD SCOUR REPORT

WBS:	TIP:	U-5025	COUNTY: Mecklenburg
			tions over Four Mile Creek in Matthews, North Carolina
		<b>EXISTING</b> I	BRIDGE
Information from:	Field Inspection _ Other (explain) _	X Micro	rofilm (reel pos:)
Bridge No.: N/A Foundation Type: N/A	Length: N/A	Total Bents: N/	A Bents in Channel: N/A Bents in Floodplain: N/A
EVIDENCE OF SCOUR Abutments or End Be	Ola NI/A		
Interior Bents: N/A			
Channel Bed: None			
Channel Bank: Relativ			
EXISTING SCOUR PRO			
Type(3): Riprap	and boulders		
Extent(4): Along	creek banks and bec	i	
Effectiveness(5): Highly	effective		
Obstructions(6): Two fa	allen trees laying acro	oss creek channe	el observed just west of Trade Street

#### **INSTRUCTIONS**

- 1 Describe the specific site's location, including route number and body of water crossed.
- 2 Note scour evidence at existing end bents or abutments (e.g. undermining, sloughing, degradations).
- 3 Note existing scour protection (e.g. rip rap).
- 4 Describe extent of existing scour protection.
- 5 Describe whether or not the scour protection appears to be working.
- 6 Note obstructions such as dams, fallen trees, debris at bents, etc.
- 7 Describe the channel bed material based on observation and/or samples. Include any lab results with report.
- 8 Describe the channel bank material based on observation and/or samples. Include any lab results with report.
- 9 Describe the material covering the banks (e.g. grass, trees, rip rap, none).
- 10 Determine the approximate floodplain width from field observation or a topographic map.
- 11 Describe the material covering the floodplain (e.g. grass, trees, crops).
- 12 Use professional judgement to specify if the stream is degrading, aggrading, or static.
- 13 Describe potential and direction of the stream to migrate laterally during the bridge's life (approx. 100 years).
- 14 Give the design scour elevation (DSE) expected over the life of the bridge (approx. 100 years). This elevation can be given as a range across the site, or for each bent. Discuss the relationship between the Hydraulics Unit theoritical scour and the DSE. If the DSE is dependent on scour counter measures, explain (e.g. rip rap armoring on slopes). The DSE is based on the erodability of materials, giving consideration to the influence of joints, foliation, bedding characteristics, % core recovery, % RQD, differential weathering, shear strength, observations at existing structures, other tests deemed appropriate, and overall geologic conditions at the site.

			<u> </u>	HUNDIN	IFORM.	<u>A HON</u>					
Channel I	Bed Material(	7): <u>Brown</u>	and Tan S	Silty Fine	to Coars	e Sand	(A-1-b)				
Channel B	ank Material(	8): <u>Brown</u>	Fine Sano	ly Silt (A	-4) and B	rown Si	lty Fine to	o Mediun	n Sand (A	\-2-4/A-2	:-5)
Channel	Bank Cover(	9): Small to	o large tre	es and i	underbrus	sh					
Flood	plain Width(1	0): 100+/-	feet on no	rth side	of creek	and 150	+/- feet o	n south :	side of cr	eek	
Flood	plain Cover(1	1): Fields a	and wood	ed areas							
	Stream is(1	2): A	\ggrading		Degra	ading	<u>X</u>	Sta	atic		
Channel Migration	n Tendency(1	3): Migratio	on tenden	cy to the	south			<del></del>			***************************************
Observations a	and Other Co	mments:									***************************************
		Reported			· · · · · · · · · · · · · · · · · · ·				<del>^</del>	3/27/2	······································
DESIGN SCOL	JR ELEVATIO	ONS(14)				Feet		Met	ers	-	
	1										
			-				ļ		ļ		
			numerous remarkations to the								
Comparison of	DSE to Hydra	aulics Unit	theoretica	l scour:							
Comparison of		Automate							Date:		
Comparison of		aulics Unit							Date:		
SOIL ANALYS	DSE de	etermined	by:						Date:		
SOIL ANALYS	DSE de IS RESULTS Creek Bed	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No.	DSE de IS RESULTS Creek Bed R-1	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4	DSE de IS RESULTS Creek Bed R-1 2	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10	DSE de IS RESULTS Creek Bed R-1 2 98	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #40	DSE de IS RESULTS Creek Bed R-1 2 98 17.2	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #40 Passed #200	DSE de IS RESULTS Creek Bed R-1 2 98 17.2 3.6	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #40	DSE de IS RESULTS Creek Bed R-1 2 98 17.2 3.6 80.8	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #40 Passed #200 Coarse Sand	DSE de IS RESULTS Creek Bed R-1 2 98 17.2 3.6	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #200 Coarse Sand Fine Sand Silt Clay	DSE de DSE de DSE de DSE de DSE de DSE de DSE de DSE dE DS	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #200 Coarse Sand Fine Sand Silt Clay LL	DSE de DSE de DSE de DSE de DSE de DSE de DSE de DSE de DSE dE DS	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #200 Coarse Sand Fine Sand Silt Clay LL PI	DSE de la RESULTS Creek Bed R-1 2 98 17.2 3.6 80.8 13.6 2.6 1 NP NP	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #200 Coarse Sand Fine Sand Silt Clay LL PI AASHTO	DSE de la RESULTS Creek Bed R-1 2 98 17.2 3.6 80.8 13.6 2.6 1 NP NP NP A-1-b	etermined	by:						Date:		
SOIL ANALYS Bed or Bank Sample No. Retained #4 Passed #10 Passed #200 Coarse Sand Fine Sand Silt Clay LL PI	DSE de la RESULTS Creek Bed R-1 2 98 17.2 3.6 80.8 13.6 2.6 1 NP NP	etermined	by:						Date:		